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Office européen des brevets



(11) Publication number : **0 577 438 A2**

(12)

EUROPEAN PATENT APPLICATION

(21) Application number : **93305235.9**

(51) Int. Cl.⁵ : **B01D 53/36, B01J 23/89**

(22) Date of filing : **02.07.93**

(30) Priority : **03.07.92 JP 200638/92**

05.10.92 JP 290760/92

15.10.92 JP 302840/92

15.10.92 JP 302891/92

15.10.92 JP 302899/92

23.10.92 JP 309433/92

13.11.92 JP 328895/92

20.11.92 JP 335478/92

24.11.92 JP 336583/92

25.12.92 JP 358235/92

25.12.92 JP 358316/92

25.12.92 JP 358348/92

13.01.93 JP 20566/93

(43) Date of publication of application :
05.01.94 Bulletin 94/01

(84) Designated Contracting States :
DE FR GB

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(54) Exhaust gas cleaner and method of cleaning exhaust gas.

(57) Nitrogen oxides are removed from an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas, by

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using an exhaust gas cleaner having Ag supported by a porous inorganic oxide body and second catalyst containing second catalytically active components supported by a porous inorganic oxide body. The second catalytically active components consist essentially of Cu and/or other metals such as alkali metal elements, rare earth elements, etc.

BACKGROUND OF THE INVENTION

The present invention relates to an exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components such as carbon monoxide, hydrogen, hydrocarbons in the exhaust gas, and a method of cleaning such an exhaust gas.

Various exhaust gases discharged from internal combustion engines such as automobile engines, etc., combustion apparatuses installed in factories, home fun heaters, etc. contain nitrogen oxides such as nitrogen monoxide, nitrogen dioxide (hereinafter referred to simply as "NOx") and oxygen in an amount larger than its stoichiometric amount relative to unburned components. The NOx is one of causes of air pollution such as photochemical smog and acidic rain, posing a serious problem of environmental pollution on a global scale. For these reasons, it is desired to remove NOx from exhaust gases emitted from various combustion equipment.

In the case of an exhaust gas from gasoline engines, NOx is usually removed by using so-called three-component catalysts. Also, in the case of large, stationary combustion apparatuses such as internal combustion engines for cogenerators, etc., ammonia is introduced into an exhaust gas, whereby nitrogen oxides in the exhaust gas are catalytically and selectively reduced.

However, in the case of an exhaust gas having a relatively high oxygen concentration such as those discharged from diesel engines and those discharged from gasoline engines operable in a lean condition, efficient removal of NOx cannot be achieved with the above-described three-component catalysts suitable for usual gasoline engines. Also, the reduction of NOx with ammonia introduced into an exhaust gas cannot be applied to movable exhaust gas sources such as automobiles, because this reduction system needs large apparatuses and poisonous, expensive ammonia.

There is an alternative method for reducing NOx, which comprises contacting an exhaust gas containing oxygen and NOx with a gaseous reducing agent such as hydrogen, carbon monoxide or hydrocarbons in the absence of a catalyst. However, since a catalyst is not used in this method, a large amount of the reducing agent should be added. Accordingly, this non-catalytic method is effective only for the exhaust gas having a relatively low oxygen concentration, which is generated by burning nearly at a theoretical air-fuel ratio.

There have been proposed methods of reducing NOx by adding to an exhaust gas a reducing agent in a larger amount than a stoichiometric amount relative to oxygen in the exhaust gas, in the presence of a catalyst such as zeolite with or without carrying a transition metal (Japanese Patent Laid-Open Nos. 63-100919, 63-283727 and 1-130735; Thesis 2A526, 1990, the 59th Spring Conference of the Japan Chemical Society; Theses 3L420, 3L422 and 3L423, 1990, the 60th Fall Conference of the Japan Chemical Society; and "Catalyst", Vol. 33, No. 2, 59 (1991)).

However, with the catalysts used in these methods, a high removal ratio of NOx cannot be achieved in a wide temperature range, and the NOx removal efficiency is poor when moisture is contained in the exhaust gas (an actual exhaust gas contains about 10% of moisture).

OBJECT AND SUMMARY OF THE INVENTION

Accordingly, an object of the present invention is to provide an exhaust gas cleaner capable of efficiently removing NOx from an exhaust gas containing nitrogen oxide and oxygen in an amount larger than the stoichiometric amount relative to unburned components such as carbon monoxide, hydrogen, hydrocarbons, etc., which is discharged from diesel engines, gasoline engines operated under oxygen excess conditions, and stationary combustion apparatuses.

Another object of the present invention is to provide a method for reducing nitrogen oxide in the exhaust gas efficiently by means of the above exhaust gas cleaner.

As a result of intense research in view of the above objects, the inventors have found that in the exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components such as carbon monoxide, hydrogen, hydrocarbons, nitrogen oxides are effectively reduced in a wide temperature range, even when the exhaust gas contains about 10% of moisture, in the presence of an exhaust gas cleaner comprising a porous inorganic oxide body and catalytically active components including silver or silver oxide and other metal or metal oxide, by adding reducing agents such as hydrocarbons and/or oxygen-containing organic compounds such as aliphatic alcohols to the exhaust gas to cause a reaction between the reducing agents and nitrogen oxides.

Thus, the first exhaust gas cleaner according to the present invention comprises a mixture of (1) a first catalyst comprising 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body; and (2) a second catalyst comprising 0.5-20 weight % (on a metal basis) of second catalytically active components supported by a porous inorganic oxide body,

the second catalytically active components consisting essentially of (i) at least one alkali metal element; (ii) at least one element selected from the group consisting of Cu, Co, Mn and V; and (iii) at least one rare earth element, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body.

5 The first method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising a mixture of (1) a first catalyst comprising 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body; and (2) a second catalyst comprising 0.5-20 weight % (on a metal basis) of second catalytically active components supported by a porous inorganic oxide body, the second catalytically active components consisting essentially of (i) at least one alkali metal element; (ii) at least one element selected from the group consisting of Cu, Co, Mn and V; and (iii) at least one rare earth element, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and (c) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides.

The second exhaust gas cleaner according to the present invention comprises a cleaner substrate made of ceramics or metals, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) the second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body.

25 The second method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising a cleaner substrate made of ceramics or metals, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) the second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and (c) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides.

40 The third exhaust gas cleaner according to the present invention comprises a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) the second catalyst comprises 2 weight % (on a metal basis) or less of a second catalytically active component supported by a porous inorganic oxide body, the second catalytically active component consisting essentially of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body.

50 The third method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) the second catalyst comprises 2 weight % (on a metal basis) or less of a second catalytically active component supported by a porous inorganic oxide body, the second catalytically active component consisting essentially of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-

containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and (c) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides, carbon monoxide and hydrocarbons.

The fourth exhaust gas cleaner according to the present invention comprises a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.2-20 weight % (on a metal basis) of first catalytically active components supported by a porous inorganic oxide body, the first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) the second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body.

The fourth method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.2-20 weight % (on a metal basis) of first catalytically active components supported by a porous inorganic oxide body, the first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) the second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and (c) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides.

The fifth method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises 0.2-20 weight % (on a metal basis) of first catalytically active components supported by a porous inorganic oxide body, the first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) the second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body; and (b) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides.

The fifth exhaust gas cleaner according to the present invention comprises catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis) of Ag, and (ii) 2 weight % or less (on a metal basis) of Cu, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body.

The sixth method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis) of Ag, and (ii) 2 weight % or less (on a metal basis) of Cu, all of the percentages being based on the total amount (100 weight %) of the porous inorganic oxide body; (b) introducing 400 volume % or less, based on the nitrogen oxides in the exhaust gas, of hydrocarbons which are gaseous in a standard state into the exhaust gas on the upstream side of the exhaust gas cleaner; and (c) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 250-600°C, thereby removing the nitrogen oxides.

The sixth exhaust gas cleaner according to the present invention comprises catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on the porous inorganic oxide body, of Ag, and (ii) 50 weight % or less (on a metal basis), based on the Ag, of at least one element selected from the group consisting of alkali metal elements and alkali earth metal elements.

The seventh method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on the porous inorganic oxide body, of Ag, and (ii) 50 weight % or less (on a metal basis), based on the Ag, of at least one element selected from the group consisting of alkali metal elements and alkali earth metal elements; and (b) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides.

The seventh exhaust gas cleaner according to the present invention comprises catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on the porous inorganic oxide body, of Ag, and (ii) 2 weight % or less (on a metal basis), based on the Ag, of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir.

The eighth method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on the Ag, of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir; and (b) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides.

The eighth exhaust gas cleaner according to the present invention comprises catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on the porous inorganic oxide body, of Ag, and (ii) 20 weight % or less (on a metal basis), based on the Ag, of at least one element selected from the group consisting of Mo, W, Cr, Ni, Mn and Co.

The ninth method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on the porous inorganic oxide body, of Ag, and (ii) 20 weight % or less (on a metal basis), based on the Ag, of at least one element selected from the group consisting of Mo, W, Cr, Ni, Mn and Co; and (b) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides.

The ninth exhaust gas cleaner according to the present invention comprises catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In.

The tenth method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas according to the present invention comprises (a) disposing an exhaust gas cleaner in a flow path of the exhaust gas, the exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, the catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (b) bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a graph showing the relation between the removal ratio of NO_x and the temperature of the exhaust gas in Example 1 and Comparative Example 1;

Fig. 2 is a graph showing the relation between the removal ratio of NO_x and the temperature of the exhaust gas in Example 2 and Comparative Example 2;

Fig. 3 is a graph showing the relation between the removal ratio of NO_x and the temperature of the exhaust gas in Example 3 and Comparative Examples 3 and 4;

Fig. 4 is a graph showing the relation between the removal ratio of NOx and the temperature of the exhaust gas in Examples 7-9 and Comparative Examples 7-8;

Fig. 5 is a graph showing the relation between the removal ratio of NOx and the temperature of the exhaust gas in Examples 10-12 and Comparative Example 9;

5 Fig. 6 is a graph showing the relation between the removal ratio of NOx and the temperature of the exhaust gas in Examples 13 and 14 and Comparative Examples 10 and 11;

Fig. 7 is a graph showing the relation between the removal ratio of NOx and the temperature of the exhaust gas in Examples 15 and 16 and Comparative Examples 12-14;

10 Fig. 8 is a graph showing the relation between the removal ratio of NOx and the temperature of the exhaust gas in Examples 17 and 18 and Comparative Examples 15 and 16; and

Fig. 9 is a graph showing the relation between the removal ratio of NOx and the temperature of the exhaust gas in Examples 19-21 and Comparative Example 17.

DETAILED DESCRIPTION OF THE INVENTION

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The present invention will be explained in detail below.

[1] First Embodiment

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[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the first embodiment comprises a mixture of a first catalyst comprising of a first catalytically active component consisting essentially of Ag; and a second catalyst comprising second catalytically active components consisting essentially of (i) at least one alkali metal element; (ii) at least one element selected from the group consisting of Cu, Co, Mn and V; and (iii) at least one rare earth element. These catalytically active components are supported by a porous inorganic oxide body.

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(a) Porous Inorganic Oxide Body

The porous inorganic oxide body serves as sites of reaction between a reducing agent and nitrogen oxides in the exhaust gas. Since the porous inorganic oxide body is exposed to a high-temperature exhaust gas, it is required to have an excellent heat resistance, and particularly an excellent thermal shock resistance. Such a porous inorganic oxide body may preferably be constituted by porous pellets or granules packed in a casing, or in the form of a solid body such as a honeycomb, a foam, a plate, or a porous inorganic oxide powder layer formed on a heat-resistant substrate.

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In the case of using the porous inorganic oxide powder layer formed on a heat-resistant substrate, the amount of the porous inorganic oxide powder is preferably 20-250 grams per 1 liter (apparent volume of substrate) (hereinafter referred to as "20 g/liter - 250 g/liter"), particularly 50 g/liter - 200 g/liter, based on the heat-resistant substrate.

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Materials for the porous inorganic oxide body include ceramics such as alumina, titania, zirconia and their composites, etc. Particularly preferable materials for the porous inorganic oxide body are γ -alumina or its composite oxide such as titania-alumina, silica-alumina, zirconia-alumina, etc. With catalytically active γ -alumina, the reducing agent added and the nitrogen oxides in the exhaust gas are reacted efficiently.

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Since NOx in the exhaust gas is reacted with a reducing agent while the exhaust gas is passing through the exhaust gas cleaner, it is preferable that the pressure drop of the exhaust gas in the exhaust gas cleaner is within a permissible range, and that the porous inorganic oxide body has a large surface area which is brought into contact with the exhaust gas. In the above respects, it is preferable that a specific surface area of the porous inorganic oxide body is about 30 m²/g or more. When the specific surface area is smaller than about 30 m²/g, a sufficient reaction between the nitrogen oxides in the exhaust gas and the reducing agent added cannot take place in the exhaust gas cleaner.

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In the case of the porous inorganic oxide layer formed on a heat-resistant substrate, the heat-resistant substrate may be made of ceramics such as alumina, silica, titania, zirconia and their composites such as silica-alumina, alumina-zirconia, alumina-titania, silica-titania, silica-zirconia, titania-zirconia, mullite, cordierite, etc. The heat-resistant substrate may be in the form of a honeycomb filter, a foam filter, a fiber assembly filter, pellets, etc.

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The porous inorganic oxide layer may be formed on the heat-resistant substrate by a known wash-coating method, a known sol-gel method, etc.

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In the wash-coating method, the heat-resistant substrate is immersed in a slurry of the above ceramic powder and dried so that a porous inorganic oxide layer is formed on the heat-resistant substrate. To cause the porous inorganic oxide layer to support a first catalytically active component comprising Ag or an oxide

thereof and a second catalytically active component comprising the other metal components (referred to simply as Ag, etc.), there are two methods available: (1) a method of applying Ag, etc. by impregnation or precipitation to the carrier layer (porous inorganic oxide layer) wash-coated on the heat-resistant substrate, and (2) a method of forming a porous inorganic oxide layer supporting Ag, etc. on the heat-resistant substrate by wash-coating the heat-resistant substrate with a suspension of ceramic powder containing Ag, etc. According to the latter method (2), the porous inorganic oxide layer supporting Ag, etc. can be formed by a single step.

In the sol-gel method, either one of the following two procedures can be conducted.

The first sol-gel method comprises hydrolyzing organic salts (for instance, alkoxides) of the porous inorganic oxide layer-constituting metals; applying the resulting sol to the heat-resistant substrate; bringing the coated heat-resistant substrate into contact with water vapor, etc. to form a layer composed of colloidal particles; drying and heating it to convert it to a carrier layer for Ag, etc.; and applying Ag, etc. to the carrier layer. For instance, when Ag, etc. are to be supported by an alumina (Al_2O_3) carrier layer, a solution of Al alkoxide (for instance, $\text{Al}(\text{o-isoC}_3\text{H}_7)_3$) in alcohol is mixed with an acid such as CH_3COOH , HNO_3 , HCl , etc. to prepare a coating solution, and the heat-resistant substrate is immersed in the coating solution. After removing the heat-resistant substrate from the coating solution, it is treated with vapor or water to cause gelation. After drying and heating, a thin alumina coating is formed on a porous surface of the heat-resistant substrate. Next, the coated heat-resistant substrate is impregnated with aqueous solutions of carbonates, nitrates, acetates, hydroxides, etc. of Ag; and the impregnated layer is dried and heated on the heat-resistant substrate.

In the second sol-gel method, the ceramic carrier materials and Ag, etc. are simultaneously applied to the heat-resistant substrate. For instance, a solution of Al alkoxide in alcohol is mixed with an acid such as CH_3COOH , HNO_3 , HCl , etc. and an aqueous solution of a silver salt to prepare a coating solution, and the heat-resistant substrate is immersed in the coating solution. After removing the heat-resistant substrate from the coating solution, it is treated with vapor or liquid water to prepare a sol, which is then converted to a gel. The gel is dried and then heated to provide a ceramic carrier supporting Ag, etc.

By using the sol-gel method, Ag, etc. can be extremely uniformly dispersed in the heat-resistant substrate, leading to an increase in catalytic activity.

In the sol-gel method, the acid serves as a hydrolysis catalyst in the course of gelation. However, alkali metals may be added in place of the acids to conduct the hydrolysis reaction.

(b) First Catalyst

The first catalyst comprises a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body. The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the total amount of the porous inorganic oxide body. When the amount of Ag or an oxide thereof is less than 0.1 weight %, sufficient effect of Ag or an oxide thereof cannot be obtained. On the other hand, even when the amount of Ag or an oxide thereof exceeds 15 weight %, further advantage of increasing the efficiency of reducing nitrogen oxides cannot be achieved. To increase the NO_x -removing efficiency, Ag or an oxide thereof added is preferably 0.5-10 weight %. Incidentally, it should be noted that when the term "Ag" is used instead of "Ag or an oxide thereof," it is intended to include a silver oxide.

With respect to the production of the exhaust gas cleaner, the porous inorganic oxide body is first immersed in an aqueous solution of a silver salt such as silver nitrate, and then dried and heated. The substrate having a porous inorganic oxide layer impregnated with Ag or an oxide thereof may also be produced under the same conditions.

The porous inorganic oxide body is preferably dried and then heated in a non-oxidizing atmosphere such as vacuum, a nitrogen atmosphere, or a hydrogen atmosphere. The drying of the porous inorganic oxide body is preferably conducted at about 70°C or higher. With respect to the heating conditions, when the heating is conducted in the above atmosphere, the resulting exhaust gas cleaners are catalytically more active than those heated in the air. Also, the heating of the exhaust gas cleaner is preferably conducted at a temperature elevating stepwise from about 100°C to about 600°C in the above non-oxidizing atmosphere, and then at about 500°C or higher in an oxygen-containing atmosphere.

The exhaust gas cleaner carrying Ag or its oxide is preferably treated with an SO_2 -containing gas. In general, 1 g of the exhaust gas cleaner carrying Ag or its oxide is brought into contact with 0.02-1 mmol of SO_2 . When the amount of SO_2 is smaller than 0.02 mmol, sufficient effect of treatment cannot be achieved. On the other hand, even when the amount of SO_2 exceeds 1 mmol, further improvement of the catalytic activity cannot be obtained.

With the exhaust gas cleaner treated with SO_2 , hydrocarbons and/or oxygen-containing organic compounds added are not directly oxidized by oxygen in the exhaust gas. Accordingly, sufficient reaction be-

tween the nitrogen oxides and the hydrocarbons and/or oxygen-containing organic compounds can proceed at such a low temperature as about 250-400°C.

(c) Second Catalyst

The second catalyst comprises second catalytically active components supported by a porous inorganic oxide body. The second catalytically active components consist essentially of (i) at least one alkali metal element (Li, Na, K, Cs, etc.); (ii) at least one element selected from the group consisting of Cu, Co, Mn and V; and (iii) at least one rare earth element (Ce, La, Nd, Sm, etc.).

The component (i) is preferably K and/or Cs. With respect to the component (ii), Cu is preferable, and one or more of the other elements (Co, Mn and V) may be added to Cu. The component (iii) may be preferably Ce and/or La. Incidentally, it should be noted that these elements exist in the form of oxides under the usual operation conditions of the exhaust gas cleaner.

The amounts of the three components (i), (ii) and (iii), respectively, expressed as weight percentage of metal elements therein, are (i) 20% or less, (ii) 60 or more %, and (ii) 20% or less, respectively based on the total amount (100 weight %) of the porous inorganic oxide body. If the components (i) and (ii) are more than 20% or if the component (iii) is less than 60%, the removal ratio of NOx at low temperatures would be low. Preferably, (i) is 15% or less, (ii) is 70% or more, and (iii) is 15% or less, and particularly (i) is 0.1-15%, (ii) is 75-99%, and (iii) is 0.1-15%.

The total amount of (i) + (ii) + (iii) is generally 0.5-20 weight %, preferably 0.5-15 weight % based on the porous inorganic oxide body. If the total amount of (i) + (ii) + (iii) is lower than 0.5 weight %, sufficient effect of carrying the second catalytic components cannot be obtained. On the other hand, if it exceeds 20 weight %, the burning of hydrocarbons would predominantly take place, resulting in the reduced removal of NOx.

(d) Ratio of First Catalyst to Second Catalyst

The mixture ratio by weight of the first catalyst to the second catalyst is preferably 5:1 - 1:5. When the first catalyst and the second catalyst are mixed at this ratio, the removal of NOx can be achieved in such a wide temperature range as 200-600°C, particularly 250-600°C. If the mixture ratio is lower than 1:5 (if the amount of the first catalyst is too small), the removal of NOx would be low in a wide temperature range of 250-600°C. On the other hand, if the mixture ratio is higher than 5:1 (if the amount of the first catalyst is too large), the removal of NOx would be low at a temperature of 400°C or lower, failing to achieve a sufficient reaction of NOx with the hydrocarbons added to the exhaust gas.

[B] Method of Cleaning Exhaust Gas

The method of the first embodiment comprises disposing the exhaust gas cleaner in a flow path of the exhaust gas; introducing reducing agents such as hydrocarbons and/or oxygen-containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides.

(a) Reducing Agents

The exhaust gas discharged from diesel engines, etc. contains small amounts of hydrocarbons such as acetylene, ethylene, propylene, etc. which can act as reducing agents for reducing the nitrogen oxides in the exhaust gas. In general, the proportion of the unburned hydrocarbons remaining in the exhaust gas is about 40 ppm, and it can be increased to some extent by adjusting engine conditions, etc. However, when hydrocarbons do not remain in the exhaust gas in sufficient amount to reduce nitrogen oxides in the exhaust gas, reducing agents such as hydrocarbons and/or oxygen-containing organic compounds are added to the exhaust gas on the upstream side of the exhaust gas cleaner in a flow path of the exhaust gas.

(1) Hydrocarbons

The hydrocarbons added to the exhaust gas may be in the form of a liquid or a gas.

The liquid hydrocarbons, which are in a liquid state in a standard state (room temperature and 1 atm), include diesel oil, cetane, heptane, kerosene, etc. The boiling point of the liquid hydrocarbon is from room temperature to about 350°C. Preferred examples of such hydrocarbons are diesel oil, cetane, heptane, etc. When a hydrocarbon having a boiling point exceeding about 450°C is added, it is not easily evaporated at an exhaust gas temperature under a normal operation condition, failing to accelerate the reduction of NOx. For safe operation, the upper limit of the boiling temperature of the liquid hydrocarbon is set at about 400°C. Preferably, a liquid hydrocarbon having a boiling point of about 350°C or lower, particularly 90-350°C is used. Such a liquid hydrocarbon is typically diesel oil, cetane, kerosene, etc., which are used as engine fuels, for a practical reason.

The gaseous hydrocarbons (alkanes, alkenes or alkynes) are in a gaseous state in a standard state. The preferred alkanes are propane, butane, etc., the preferred alkenes are ethylene, propylene, bu-

tylene, etc., and the preferred alkynes are acetylene, etc.

(2) Oxygen-Containing Organic Compounds

The oxygen-containing organic compounds have 2 or more carbon atoms and 1 or more oxygen atoms. Specific examples of such oxygen-containing organic compounds include alcohols, ketones, aldehydes, carboxylic acids, ethers, esters, etc. The upper limit of the carbon number in the oxygen-containing organic compound is preferably determined such that the boiling point of the oxygen-containing organic compound does not exceed 400°C.

(i) Alcohols

As alcohols, monovalent aliphatic alcohols having low molecular weights such as ethanol, propanol (n-propyl alcohol, isopropyl alcohol), etc. are preferable. However, methanol is not effective to react with nitrogen oxides. Accordingly, the carbon number of the aliphatic alcohol is preferably restricted to 2 or more.

(ii) Ketones

As ketones, acetone may be used.

(iii) Carboxylic Acids

As carboxylic acids, acetic acid is particularly preferable.

(iv) Aldehydes

As aldehydes, acetaldehyde is particularly preferable.

(3) Amount of Reducing Agent Added

The amount of the hydrocarbon and/or the oxygen-containing organic compound added is properly determined depending on the amount of NO_x in the exhaust gas. Specifically, a weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is 0.2-5. When the weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x is less than 0.2, sufficient effect of adding the hydrocarbon and/or the oxygen-containing organic compound cannot be obtained. The upper limit of the weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x is determined from the economic point of view. The preferred weight ratio is 0.2-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C. When the temperature of the exhaust gas is lower than 200°C, a sufficient reaction between the nitrogen oxides and hydrocarbon and/or oxygen-containing organic compound cannot proceed. On the other hand, when the temperature of the exhaust gas is higher than 600°C, the hydrocarbon and/or oxygen-containing organic compound is burned, failing to reduce the nitrogen oxides effectively. The more preferred temperature of the exhaust gas is 250-600°C.

(c) Contact Time

How long it takes for the exhaust gas to pass through the exhaust gas cleaner is expressed by a product of a time period during which a unit amount of the exhaust gas is in contact with the exhaust gas cleaner and the amount of the catalyst. This product is defined as "contact time." The unit of the contact time is sec-g/ml, wherein "g" is a weight of the exhaust gas cleaner, and "ml/sec" is a volume of the exhaust gas which comes into contact with the catalyst per a second (converted to a volume in a standard state of 1 atm and room temperature). For instance, when 1 ml/sec (converted to a volume in a standard state) of an exhaust gas is brought into contact with 1 g of the catalyst for 0.03 seconds, the contact time is 0.03 sec-g/ml.

In the first embodiment, the contact time is 0.006 sec-g/ml or more. When the contact time is less than 0.006 sec-g/ml, a sufficient reaction does not take place between the nitrogen oxides and the reducing agent, resulting in a low removal ratio of nitrogen oxides. Also, the unreacted reducing agent remains in the exhaust gas which is to be discharged.

On the other hand, when the contact time is too large, the exhaust gas cleaner becomes too large. Accordingly, the upper limit of the contact time is preferably 0.5 sec-g/ml.

[2] Second Embodiment

[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the second embodiment comprises a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) the second catalyst comprises a second catalytically active component consisting essentially of Cu supported by

a porous inorganic oxide body. The second catalytically active component may further contain at least one element selected from the group consisting of alkali metal elements and rare earth elements.

(a) Cleaner Substrate

The cleaner substrate may be made of ceramics such as γ -alumina and composite oxides thereof (titanium-alumina, silica-alumina, zirconia-alumina, etc.). When high heat resistance is required, cordierite and mullite may also be used. In addition, known heat-resistant metals such as stainless steel, etc. may be used for the cleaner substrate.

The size and shape of the cleaner substrate may be changed depending on the purposes. For practical reason, the cleaner substrate preferably consists of two parts arranged on the inlet side and the outlet side. The internal structure of the cleaner substrate is honeycomb, foam, fibrous, or other three-dimensional structure. Also, the outer structure of the cleaner substrate may be a plate, a disc, a pellet, etc.

(b) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the second embodiment is preferably in the form of fine powder which can be coated onto the cleaner substrate. The materials for the porous inorganic oxide powder may be the same as in the first embodiment. The amount of the porous inorganic oxide powder is preferably 20 g/liter - 250 g/liter, particularly 50 g/liter - 200 g/liter, based on the heat-resistant cleaner substrate.

The porous inorganic oxide powder layer may be formed on the heat-resistant cleaner substrate by the same method as described in the first embodiment.

(c) First Catalyst

The first catalyst comprises a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide powder. The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the total amount of the porous inorganic oxide powder. To increase the NO_x-removing efficiency, Ag or an oxide thereof added is preferably 0.5-10 weight %.

The cleaner substrate having a porous inorganic oxide layer impregnated with Ag or an oxide thereof may be produced in the same manner as in the first embodiment. Incidentally, the exhaust gas cleaner carrying Ag or its oxide is preferably treated with an SO₂-containing gas.

(d) Second Catalyst

The second catalyst comprises second catalytically active components supported by a porous inorganic oxide body. The second catalytically active component consists essentially of Cu. The amounts of Cu, expressed as a weight percentage of a metal element itself, is 0.1-15%. If Cu is less than 0.1% or more than 15%, the removal ratio of NO_x would be low. The preferred amount of Cu is 0.5-12%.

The second catalyst may be a combination of Cu and at least one element selected from the group consisting of alkali metal elements and rare earth elements. The alkali metal element may be Li, Na, K, Cs, etc., preferably K and/or Cs, and the rare earth element may be Ce, La, Nd, Sm, etc., preferably Ce and/or La.

The total amount of the alkali metal element and the rare earth element is 4 weight % or less, preferably 0.5-3 weight %. Further, the amount of the alkali metal element is preferably 2 weight % or less, and the amount of the rare earth element is preferably 2 weight % or less. If both of the alkali metal element and the rare earth element are more than 2 weight %, the removal ratio of NO_x would be low. More preferably, each of the alkali metal element and the rare earth element is 0.1-1.5 weight %.

The total amount of (i) Cu + (ii) alkali metal element and/or rare earth element is generally 0.1-19 weight %, preferably 0.5-15 weight % based on the porous inorganic oxide body. If the total amount of (i) + (ii) is lower than 0.1 weight %, sufficient effect of carrying the second catalytic components cannot be obtained. On the other hand, if it exceeds 19 weight %, the burning of hydrocarbons would predominantly take place, resulting in the reduced removal of NO_x.

Incidentally, the second catalyst may be supported by the cleaner substrate in the same manner as the first catalyst.

(e) Arrangement of First Catalyst to Second Catalyst

In the second embodiment, the first catalyst is disposed on the exhaust gas inlet side, and the second catalyst is disposed on the exhaust gas outlet side in the exhaust gas cleaner. With this arrangement, high removal ratio of NO_x can be achieved.

(f) Ratio of First Catalyst to Second Catalyst

The ratio by weight of the first catalyst to the second catalyst is preferably 5:1 - 1:5. When the first catalyst and the second catalyst are arranged at this ratio, the removal of NO_x can be achieved in such a wide temperature range as 200-600°C, particularly 250-600°C for the reason as mentioned in the first embodiment.

[B] Method of Cleaning Exhaust Gas

The method of the second embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; introducing hydrocarbons and/or oxygen-containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides.

(a) Reducing Agents

The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds may be the same as in the first embodiment. A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 0.2-5. The preferred weight ratio is 0.2-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C. The more preferred temperature of the exhaust gas is 250-600°C.

(c) Contact Time

The contact time may be the same as in the first embodiment.

[3] Third Embodiment

[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the third embodiment comprises a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) the second catalyst comprises a second catalytically active component supported by a porous inorganic oxide body, the second catalytically active component consisting essentially of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir.

(a) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the third embodiment may be the same as in the first embodiment. The amount of the porous inorganic oxide powder is preferably 20 g/liter - 250 g/liter, particularly 50 g/liter - 200 g/liter, based on a heat-resistant cleaner substrate, if any. The porous inorganic oxide powder layer may be formed on the heat-resistant cleaner substrate by the same method as described in the first embodiment.

(b) First Catalyst

The first catalyst comprises a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide powder. The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the total amount of the porous inorganic oxide powder. To increase the NO_x-removing efficiency, Ag or an oxide thereof added is preferably 0.5-10 weight %.

The cleaner substrate having a porous inorganic oxide layer impregnated with Ag or an oxide thereof may be produced in the same manner as in the first embodiment. Incidentally, the exhaust gas cleaner carrying Ag or its oxide is preferably treated with an SO₂-containing gas.

(c) Second Catalyst

The second catalyst comprises second catalytically active components supported by a porous inorganic oxide body. The second catalytically active component consists essentially of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir. The amounts of the second catalytically active component, expressed as a weight percentage of a metal element itself, is 2% or less, preferably 0.1-1.5%. The second catalyst may be prepared in the same manner as the first catalyst.

The second catalyst preferably further contains at least one rare earth element such as La, Ce, etc. in an amount of 10 weight % or less. With the rare earth element, the heat resistance of Pt, etc. can be increased.

(d) Arrangement of First Catalyst to Second Catalyst

In the third embodiment, the first catalyst is disposed on the exhaust gas inlet side, and the second catalyst is disposed on the exhaust gas outlet side in the exhaust gas cleaner. With this arrangement, high removal ratio of NO_x can be achieved.

(e) Ratio of First Catalyst to Second Catalyst

The ratio by weight of the first catalyst to the second catalyst is preferably 5:1 - 1:5. When the first catalyst and the second catalyst are arranged at this ratio, the removal of NO_x can be achieved in such a wide temperature range as 200-600°C, particularly 250-600°C even when about 10% of water is con-

tained in the exhaust gas. The more preferred ratio is 4:1 - 1:4.

[B] Method of Cleaning Exhaust Gas

The method of the third embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; introducing hydrocarbons and/or oxygen-containing organic compounds into the exhaust gas on the upstream side of the exhaust gas cleaner; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides.

(a) Reducing Agents

The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds added to the exhaust gas may be the same as in the first embodiment.

A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 0.1-5 as in the first embodiment. The preferred weight ratio is 0.2-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C. The more preferred temperature of the exhaust gas is 300-600°C.

(c) Contact Time

The contact time may be the same as in the first embodiment.

[4] Fourth Embodiment

[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the fourth embodiment comprises a cleaner substrate, a first catalyst supported by the cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by the cleaner substrate on the exhaust gas outlet side thereof, wherein (1) the first catalyst comprises first catalytically active components supported by a porous inorganic oxide body, the first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) the second catalyst comprises a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body.

(a) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the fourth embodiment may be the same as in the first embodiment. The porous inorganic oxide powder layer may be formed on the heat-resistant cleaner substrate by the same method as described in the first embodiment.

(b) First Catalyst

The first catalyst comprises first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In. The total amount of the first catalytically active components is generally 0.2-20 weight % (on a metal basis) based on the total amount of the porous inorganic oxide powder. The preferred total amount of the first catalytically active components is 0.5-15 weight %.

Among the first catalytically active components, Ag or an oxide thereof is preferably 0.1-10 weight % (on a metal basis), and at least one element selected from the group consisting of Sn, Al, Ga and In is preferably 0.1-10 weight % (on a metal basis), each based on the total amount of the porous inorganic oxide powder. Incidentally, silver may exist in the form of a metal or an oxide, and Sn, etc. may exist in the form of an oxide at the exhaust gas temperature.

The cleaner substrate having a porous inorganic oxide layer impregnated with Ag and Sn, etc. may be produced in the same manner as in the first embodiment. Incidentally, the exhaust gas cleaner carrying Ag or its oxide is preferably treated with an SO₂-containing gas.

(c) Second Catalyst

The second catalyst comprises a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body. The second catalytically active component may further contain at least one element selected from the group consisting of alkali metal elements and rare earth elements as in the second embodiment. The alkali metal element may be Li, Na, K, Cs, etc., preferably K and/or Cs, and the rare earth element may be Ce, La, Nd, Sm, etc., preferably Ce and/or La.

The amount of Cu is 0.1-15 weight %. If Cu is less than 0.1 weight % or more than 15 weight %, the removal ratio of NO_x would be low. The preferred amount of Cu is 0.5-12 weight %.

When the alkali metal element and the rare earth element are added, the total amount thereof is 4 weight % or less, preferably 0.2-3 weight %. Further, the amount of the alkali metal element is preferably

0.01-2 weight %, and the amount of the rare earth element is preferably 0.01-2 weight %. If both of the alkali metal element and the rare earth element are more than 2 weight %, the removal ratio of NO_x would be low. More preferably, each of the alkali metal element and the rare earth element is 0.1-1.5 weight %.

The total amount of (i) Cu + (ii) alkali metal element and/or rare earth element is generally 0.1-19 weight %, preferably 0.5-15 weight % based on the porous inorganic oxide body. If the total amount of (i) + (ii) is lower than 0.1 weight %, sufficient effect of carrying the second catalytic components cannot be obtained. On the other hand, if it exceeds 19 weight %, the burning of hydrocarbons would predominantly take place, resulting in the reduced removal of NO_x.

Incidentally, the second catalyst may be prepared in the same manner as the first catalyst.

(d) Arrangement of First Catalyst to Second Catalyst

In the fourth embodiment, the first catalyst is disposed on the exhaust gas inlet side, and the second catalyst is disposed on the exhaust gas outlet side in the exhaust gas clearer. With this arrangement, high removal ratio of NO_x can be achieved.

(e) Ratio of First Catalyst to Second Catalyst

The ratio by weight of the first catalyst to the second catalyst is preferably 5:1 - 1:5. The more preferred ratio is 4:1 - 1:4. With this combination, high removal ratio can be achieved even when about 10% of water is contained in the exhaust gas.

[B] Method of Cleaning Exhaust Gas

The method of the fourth embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby removing the nitrogen oxides. The hydrocarbons and/or oxygen-containing organic compounds may be introduced into the exhaust gas on the upstream side of the exhaust gas cleaner to increase the removal ratio of NO_x.

(a) Reducing Agents

The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds added to the exhaust gas may be the same as in the first embodiment.

A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 0.1-5 as in the first embodiment. The preferred weight ratio is 0.2-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C. The more preferred temperature of the exhaust gas is 300-600°C.

(c) Contact Time

The contact time may be the same as in the first embodiment.

[5] Fifth Embodiment

[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the fifth embodiment comprises catalytically active components consisting essentially of a mixture of Ag and Cu supported by a porous inorganic oxide body.

(a) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the fifth embodiment may be the same as in the first embodiment. The porous inorganic oxide powder layer may be formed on the heat-resistant cleaner substrate by the same method as described in the first embodiment.

(b) Ag

The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the amount of the porous inorganic oxide body. The preferred amount of Ag is 0.5-10 weight %.

(c) Cu

The amount of Cu is 2 weight % or less based on the porous inorganic oxide body. The preferred amount of Cu is 0.001-2 weight %.

(d) Arrangement of Ag and Cu

Ag and Cu are supported by the porous inorganic oxide body in the form of a mixture. Ag and Cu may be carried by an impregnation method, etc. using aqueous solutions of Ag and Cu. Except for the mixture form, the exhaust gas cleaner of the fifth embodiment may be produced in the same manner as described above.

[B] Method of Cleaning Exhaust Gas

The method of the fifth embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; introducing 400 volume % or less, based on the nitrogen oxides in the exhaust gas, of hydrocarbons which are gaseous in a standard state into the exhaust gas on the upstream side of said exhaust gas cleaner; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 250-600°C, thereby removing the nitrogen oxides.

(a) Gaseous Hydrocarbons

The gaseous hydrocarbons added to the exhaust gas may be the same as in the first embodiment.

The gaseous hydrocarbon is preferably 400 volume % or less based on the amount of NO_x in the exhaust gas. If more than 400 volume % of the gaseous hydrocarbon is added, excess gaseous hydrocarbon may remain in the exhaust gas. The preferred amount of gaseous hydrocarbon is 300 volume % or less.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 250-600°C. When the gaseous hydrocarbon is alkane or alkene, the temperature of the exhaust gas is preferably 300-600°C. When alkyne is added together with alkane or alkene, the temperature of the exhaust gas is preferably 250-600°C.

(c) Contact Time

The contact time may be the same as in the first embodiment.

[6] Sixth Embodiment

[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the sixth embodiment comprises catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of alkali metal elements and alkali earth metal elements.

(a) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the sixth embodiment may be the same as in the first embodiment.

(b) Ag

The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the amount of the porous inorganic oxide body. The preferred amount of Ag is 0.5-10 weight %.

(c) Alkali Metal Elements and/or Alkali Earth Metal Elements

The alkali metal elements are Li, Na, K, Cs, etc., preferably K and/or Cs. The alkali earth metal elements are preferably Ca, Sr, Ba. The total amount of the alkali metal elements and/or the alkali earth metal elements is 50 weight % or less based on the amount of Ag. If it is more than 50 weight %, the removal ratio of NO_x would be low. The lower limit of the total amount of the alkali metal elements and/or the alkali earth metal elements is 0.001 weight %. Incidentally, these elements may exist in the form of oxide at the exhaust gas temperature.

(d) Arrangement of Ag and Alkali Metal Elements and/or Alkali Earth Metal Elements

Ag and the alkali metal elements and/or the alkali earth metal elements are supported by the porous inorganic oxide body in the form of a mixture. They may be carried by an impregnation method, etc. using their aqueous solutions. Except for the mixture form, the exhaust gas cleaner of the sixth embodiment may be produced in the same manner as described above.

[B] Method of Cleaning Exhaust Gas

The method of the sixth embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides. The hydrocarbons and/or oxygen-containing organic compounds in amounts of 5 times or less those of the nitrogen oxides in the exhaust gas may be introduced into the exhaust gas on the upstream side of the exhaust gas cleaner.

(a) Reducing Agents

The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds may be the same as in the first embodiment. A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 5 or less. The more preferred weight ratio is 0.2-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C, preferably 300-600°C.

(c) Contact Time

5 The contact time may be the same as in the first embodiment.

[7] Seventh Embodiment

[A] Exhaust Gas Cleaner

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The exhaust gas cleaner of the seventh embodiment comprises catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir.

(a) Porous Inorganic Oxide Body

15 The porous inorganic oxide body used in the seventh embodiment may be the same as in the first embodiment.

(b) Ag

The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the amount of the porous inorganic oxide body. The preferred amount of Ag is 0.5-10 weight %.

(c) Pt, Pd, Ru, Rh and/or Ir

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The amount of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir is 2 weight % or less based on the amount of Ag. If it is more than 2 weight %, the removal ratio of NO_x would be low. The lower limit of the amount of Pt, etc. is 0.001 weight %. The preferred amount of Pt, etc. is 0.005-2 weight %.

(d) Arrangement of Ag and Pt, etc.

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Ag and Pt, etc. are supported by the porous inorganic oxide body in the form of a mixture. They may be carried by an impregnation method, etc. using their aqueous solutions. Except for the mixture form, the exhaust gas cleaner of the seventh embodiment may be produced in the same manner as described above.

30 [B] Method of Cleaning Exhaust Gas

The method of the seventh embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides. The hydrocarbons and/or oxygen-containing organic compounds in amounts of 5 times or less those of the nitrogen oxides in the exhaust gas may be introduced into the exhaust gas on the upstream side of the exhaust gas cleaner.

35

(a) Reducing Agents

40 The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds may be the same as in the first embodiment. A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 5 or less. The more preferred weight ratio is 0.1-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C, preferably 300-600°C.

45

(c) Contact Time

The contact time may be the same as in the first embodiment.

[8] Eighth Embodiment

50 [A] Exhaust Gas Cleaner

The exhaust gas cleaner of the eighth embodiment comprises catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Mo, W, Cr, Ni, Mn and Co.

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(a) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the eighth embodiment may be the same as in the first embodiment.

(b) Ag

The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the

amount of the porous inorganic oxide body. The preferred amount of Ag is 0.5-10 weight %.

(c) Mo, W, Cr, Ni, Mn and/or Co

Among them, Mo, W and Cr are preferable. The amount of Mo, etc. is 20 weight % or less based on the amount of Ag. If it is more than 20 weight %, the removal ratio of NO_x would be low. The lower limit of the amount of Mo, etc. is 0.05 weight %. The preferred amount of Mo, etc. is 0.1-18 weight %.

(d) Arrangement of Ag and Mo, etc.

Ag and Mo, etc. are supported by the porous inorganic oxide body in the form of a mixture. They may be carried by an impregnation method, etc. using their aqueous solutions. Except for the mixture form, the exhaust gas cleaner of the seventh embodiment may be produced in the same manner as described above.

[B] Method of Cleaning Exhaust Gas

The method of the eighth embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides. The hydrocarbons and/or oxygen-containing organic compounds in amounts of 5 times or less those of the nitrogen oxides in the exhaust gas may be introduced into the exhaust gas on the upstream side of the exhaust gas cleaner.

(a) Reducing Agents

The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds may be the same as in the first embodiment. A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 5 or less. The more preferred weight ratio is 0.1-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C, preferably 300-600°C.

(c) Contact Time

The contact time may be the same as in the first embodiment.

[9] Ninth Embodiment

[A] Exhaust Gas Cleaner

The exhaust gas cleaner of the ninth embodiment comprises catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In.

(a) Porous Inorganic Oxide Body

The porous inorganic oxide body used in the ninth embodiment may be the same as in the first embodiment.

(b) Ag

The amount of Ag or an oxide thereof is generally 0.1-15 weight % (on a metal basis) based on the amount of the porous inorganic oxide body. The preferred amount of Ag is 0.5-10 weight %.

(c) Sn, Al, Ga and/or In

The amount of Sn, etc. is 0.2-20 weight % based on the amount of the porous inorganic oxide body. The preferred amount of Sn, etc. is 0.5-15 weight %.

(d) Arrangement of Ag and Sn, etc.

Ag and Sn, etc. are supported by the porous inorganic oxide body in the form of a mixture. They may be carried by an impregnation method, etc. using their aqueous solutions.

(e) Ratio of Ag to Sn, etc.

The ratio by weight of Ag to Sn, etc. is preferably 5:1 - 1:5. The more preferred ratio is 4:1 - 1:4.

[B] Method of Cleaning Exhaust Gas

The method of the ninth embodiment comprises disposing an exhaust gas cleaner in a flow path of the exhaust gas; and bringing the exhaust gas into contact with the exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between the nitrogen oxides and hydrocarbons remaining in the exhaust gas to remove the nitrogen oxides. The hydrocarbons and/or oxygen-containing organic compounds in amounts of 0.1-5 times those of the nitrogen oxides in the exhaust gas may be introduced into the exhaust gas on the upstream side of the exhaust gas cleaner.

(a) Reducing Agents

The reducing agents such as hydrocarbons and/or oxygen-containing organic compounds may be the same as in the first embodiment. A weight ratio of the hydrocarbon and/or the oxygen-containing organic compound to NO_x in the exhaust gas is preferably 0.1-5. The more preferred weight ratio is 0.1-3.

(b) Temperature of Exhaust Gas

The exhaust gas passing through the exhaust gas cleaner is kept at a temperature of 200-600°C, preferably 250-600°C.

(c) Contact Time

The contact time may be the same as in the first embodiment.

Incidentally, in the above explanations, the catalytically active components are expressed as metal elements themselves such as Ag, Cu, etc. for simplicity, but it should be noted that these catalytically active components may exist in the form of oxide. Therefore, it is intended that the catalytically active components expressed only by metal elements include their oxides.

The present invention will be described in further detail by way of the following Examples. In each Example and Comparative Example, the catalytically active components are expressed as metal elements simplicity, and the amounts of the catalytically active components are expressed on a metal basis.

Example 1

Commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in an aqueous solution of AgNO₃, dried at 70°C and heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in a nitrogen stream containing 5 volume % of hydrogen and finally at 500°C for 2 hours in a nitrogen stream containing 10 volume % of oxygen, to obtain a first cleaner portion in which 2 weight % (on a metal basis) of Ag was supported by the γ -alumina pellets.

Commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in an aqueous solution of Cu(NO₃)₂, an aqueous solution of La(NO₃)₃, and an aqueous solution of CsNO₃, respectively to impregnate the pellets with 10.0 weight % (on a metal basis) of Cu(NO₃)₂, 0.4 weight % (on a metal basis) of La(NO₃)₃ and 0.4 weight % (on a metal basis) of CsNO₃, each based on γ -alumina. The pellets were dried and heated at 700°C to provide a second cleaner portion. Incidentally, Cu, La and Cs exited in the form of oxides in the second cleaner portion.

The first and second cleaner portions were mixed with each other at a weight ratio of 1:1, and 1.34 g of the resulting mixture was charged into a reactor pipe.

Next, a test gas having a composition shown in Table 1 below was caused to pass through the reactor pipe at a rate of 1.75 liters per minute (in a standard state), which corresponded to a space velocity of 30,000 h⁻¹ and a contact time of 0.05 sec·g/ml. The temperature of the test gas was kept at 200-550°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene.

Table 1

Component	Concentration
Nitrogen monoxide	800 ppm
Carbon dioxide	10 volume %
Oxygen	10 volume %
Propylene	1714 ppm
Nitrogen	Balance
Water	10 volume % based on the total (100 volume %) of the above components.

By passing through the reactor pipe, nitrogen monoxide was converted to nitrogen and nitrogen dioxide. Accordingly, the concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. Incidentally, the removal ratio of NO_x was calculated from the amount (X_a) of NO_x in exhaust gas before entering into the filter, and the amount of (X_b) of NO_x in exhaust gas after passage through the filter, by using the formula: $[(X_a - X_b) / X_a] \times 100\%$. The results are shown in Fig. 1.

Comparative Example 1

With the first cleaner portion used in Example 1 (porous γ -alumina pellets carrying Ag) only, the same procedures as in Example 1 were conducted to measure the removal ratio of NOx. The results are shown in Fig. 1.

Example 2

With a test gas having a composition shown in Table 2 below, Example 1 was repeated to measure the removal ratio of NOx. The results are shown in Fig. 2.

Table 2

Component	Concentration
Nitrogen monoxide	800 ppm
Carbon dioxide	10 volume %
Oxygen	10 volume %
Diesel oil	3 times the weight of NO
Nitrogen	Balance
Water	10 volume % based on the total (100 volume %) of the above components.

Comparative Example 2

With the cleaner used in Comparative Example 1, the same procedures as in Example 1 were conducted by using the test gas having a composition shown in Table 2 to measure the removal ratio of NOx. The results are shown in Fig. 2.

As is clear from Figs. 1 and 2, the NOx was well removed in such a wide temperature range as 250-550°C in Examples 1 and 2, while the removal ratio of NOx was extremely low at an exhaust gas temperature of 400°C or lower in Comparative Examples 1 and 2.

Example 3

Porous γ -Al₂O₃ powder was impregnated with 5 weight % of Ag by using an aqueous solution of AgNO₃, and a commercially available honeycomb-type cordierite filter (diameter: 20 mm, thickness: about 8.4 mm, specific surface area: 200 m²/g) was coated with about 0.5 g of the above γ -Al₂O₃ powder carrying Ag, dried and heated at a temperature up to 600°C to obtain a first cleaner portion.

Similarly, γ -Al₂O₃ powder was impregnated with 10.0 weight % of Cu by using an aqueous solution of Cu(NO₃)₂, 0.4 weight % of La by using an aqueous solution of La(NO₃)₃, and 0.4 weight % of Cs by using an aqueous solution of CsNO₃. 0.5 g of this γ -Al₂O₃ carrying Cu, La and Cs was applied to a similar honeycomb-type cordierite filter, dried and heated at a temperature up to 600°C to obtain a second cleaner portion.

The first and second cleaner portions were set in a reactor pipe such that the first cleaner portion carrying the silver catalyst was disposed on the exhaust gas inlet side, and the second cleaner portion carrying the copper-based catalyst was disposed on the exhaust gas outlet side.

Next, a test gas having a composition shown in Table 3 below was caused to pass through the reactor pipe at a rate of 2.4 liters per minute (in a standard state), which corresponded to a space velocity of 56,000 h⁻¹ and a contact time of 0.013 sec-g/ml.

Table 3

Component	Concentration
Nitrogen monoxide	800 ppm
Oxygen	10 volume %
Propylene	1714 ppm
Nitrogen	Balance
Water	10 volume % based on the total (100 volume %) of the above components.

The temperature of the test gas was kept at 200-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene. The concentration of NOx (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NOx. The results are shown in Fig. 3.

Comparative Example 3

A commercially available honeycomb-type cordierite filter (diameter: 20 mm, thickness: about 16.8 mm, specific surface area: 200 m²/g) was coated with 1 g of a first catalyst layer of Example 3 consisting of porous γ -Al₂O₃ powder and silver, and charged into a reactor pipe in the same manner as in Example 3 to measure the removal ratio of NOx. The results are shown in Fig. 3.

Comparative Example 4

A commercially available honeycomb-type cordierite filter (diameter: 20 mm, thickness: about 16.8 mm, specific surface area: 200 m²/g) was coated with 1 g of a second catalyst layer of Example 3 consisting of porous γ -Al₂O₃ powder and Cu, La and Cs, and charged into a reactor pipe in the same manner as in Example 3 to measure the removal ratio of NOx. The results are shown in Fig. 3.

As is clear from Fig. 3, the NOx was well removed in a wide temperature range in Example 3, while the removal ratio of NOx was extremely low at an exhaust gas temperature of 400°C or lower in Comparative Example 3. Also, in Comparative Example 4, the removal ratio of NOx was extremely low in a wide temperature range.

Example 4

10 g of commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in an aqueous solution of AgNO₃, dried and heated at temperatures up to 600°C stepwise to obtain a first cleaner portion in which 2 weight % (on a metal basis) of Ag was supported by the γ -alumina pellets. 2 g of similar commercially available γ -alumina pellets were immersed in an aqueous solution of chloroplatinic acid to impregnate the pellets with 0.2 weight % of Pt. After drying, the pellets were heated at temperatures up to 700°C to obtain a second cleaner portion.

The first and second cleaner portions were set in a reactor pipe such that 10 g of the first cleaner portion containing the silver catalyst was disposed on the exhaust gas inlet side, and 1 g of the second cleaner portion containing the Pt catalyst was disposed on the exhaust gas outlet side.

Next, a test gas having a composition shown in Table 4 below was caused to pass through the reactor pipe at a rate of 2.0 liters per minute (in a standard state), which corresponded to a space velocity of 8,000 h⁻¹, a silver catalyst contact time of 0.3 sec·g/ml, and a Pt catalyst contact time of 0.03 sec·g/ml. The temperature of the test gas was kept at 200-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene.

Table 4

Component	Concentration
Nitrogen monoxide	500 ppm
Carbon monoxide	100 ppm
Oxygen	10 volume %
Propylene	500 ppm
Nitrogen	Balance
Water	10 volume % based on the total (100 volume %) of the above components.

The concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. The results are shown in Table 5.

Example 5

Porous γ -Al₂O₃ powder (specific surface area: 200 m²/g) was impregnated with 2 weight % of Ag by using an aqueous solution of AgNO₃, and a commercially available honeycomb-type cordierite filter (diameter: 20 mm, thickness: about 30 mm) was coated with about 0.3 g of the above γ -Al₂O₃ powder carrying Ag, dried and heated at temperatures up to 600°C stepwise to obtain a first cleaner portion. Similarly, γ -Al₂O₃ powder was impregnated with 0.2 weight % of Pd by using an aqueous solution of palladium chloride, and 0.25 g of this γ -Al₂O₃ carrying Pd was applied to a similar honeycomb-type cordierite filter (diameter: 20 mm, thickness: about 8.4 mm), dried and heated at a temperature up to 700°C to obtain a second cleaner portion. The first and second cleaner portions were set in a reactor pipe such that the silver catalyst was disposed on the exhaust gas inlet side, and the Pd catalyst was disposed on the exhaust gas outlet side.

Next, a test gas having a composition shown in Table 4 was caused to pass through the reactor pipe at an apparent space velocity of 10,000 h⁻¹. The results are shown in Table 5.

Example 6

Spherical titania pellets (diameter: 3 mm, and specific surface area: 200 m²/g) were impregnated with 0.2 weight % of Pt and 0.02 weight % of Rh in the same manner as in Example 4, and 1 g of the titania pellets carrying Pt and Rh were combined with 10 g of the first cleaner portion containing the silver catalyst used in Example 4 and set in a reactor pipe such that the silver catalyst was disposed on the exhaust gas inlet side, and the Pt/Rh catalyst was disposed on the exhaust gas outlet side. With the above exhaust gas cleaner, the removal ratio of NO_x was measured with the test gas having a composition shown in Table 4. The results are shown in Table 5.

Comparative Example 5

11 g of pellets made of porous γ -alumina carrying 0.2 weight % of Pt were set in a reactor pipe in the same manner as in Example 4 to measure the removal ratio of NO_x from a test gas having a composition shown in Table 4. The results are shown in Table 5.

Comparative Example 6

11 g of pellets made of porous γ -alumina carrying 2 weight % of Ag were set in a reactor pipe in the same manner as in Example 4 to measure the removal ratio of NO_x from a test gas having a composition shown in Table 4. The results are shown in Table 5.

Table 5

Removal Ratios of NOx, CO and HC						
Reaction Temp.	Component Removed	Removal Ratio (%)				
		Ex.4	Ex.5	Ex.6	Com.Ex.5	Com.Ex.6
250°C	NOx	23	20	25	15	5
	CO	85	100	70	70	60
	HC	60	65	50	55	45
300°C	NOx	28	25	30	20	10
	CO	95	100	80	95	70
	HC	65	70	55	50	50
400°C	NOx	55	53	58	2	60
	CO	100	100	100	100	88
	HC	98	96	98	80	75
500°C	NOx	65	64	65	1	68
	CO	100	100	100	100	90
	HC	100	100	100	100	85
550°C	NOx	45	45	43	1	45
	CO	100	100	100	100	95
	HC	100	100	100	100	90

As is clear from the above, the NOx was well removed in a wide temperature range and carbon monoxide and carbon hydroxide were also effectively removed in Examples 4-6. On the other hand, a temperature range in which the removal ratio of NOx was high was narrow in Comparative Examples 5 and 6.

Example 7

Porous γ -Al₂O₃ powder (specific surface area: 200 m²/g) was impregnated with 2 weight % of Ag and 1 weight % of In by using an aqueous solution of silver nitrate and an aqueous solution of indium nitrate, and a commercially available honeycomb-type cordierite filter (diameter: 20 mm, thickness: about 8.4 mm) was coated with 0.52 g of the above γ -Al₂O₃ powder carrying Ag and In, dried and heated at a temperature up to 600°C stepwise to obtain a first cleaner portion. Similarly, γ -Al₂O₃ powder was impregnated with 10.0 weight % of Cu by using an aqueous solution of copper nitrate, 0.4 weight % of La by using an aqueous solution of lanthanum nitrate, and 0.4 weight % of Cs by using an aqueous solution of cesium nitrate, and 0.52 g of this γ -Al₂O₃ carrying Cu, La and Cs was applied to a similar honeycomb-type filter (diameter: 20 mm, thickness: about 8.4 mm), dried and heated at a temperature up to 700°C to obtain a second cleaner portion.

The first and second cleaner portions were set in a reactor pipe such that the silver-based catalyst was disposed on the exhaust gas inlet side, and the Cu-based catalyst was disposed on the exhaust gas outlet side.

Next, a test gas having a composition shown in Table 3 below was caused to pass through the reactor pipe at a rate of 2.43 liters per minute (in a standard state), which corresponded to an apparent space velocity of 28,000 h⁻¹, a silver catalyst contact time of 0.13 sec·g/ml, and a Cu-based catalyst contact time of 0.13 sec·g/ml.

The temperature of the test gas was kept at 200-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene. The concentration of NOx (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chem-

luminescence analyzer to determine the removal ratio of NOx. The results are shown in Fig. 4.

Example 8

5 Porous γ -Al₂O₃ powder (specific surface area: 200 m²/g) was impregnated with 2 weight % of Ag by using an aqueous solution of AgNO₃, and 1 weight % of Sn by using a solution of stannous chloride in ethyl alcohol, and the same honeycomb-type cordierite filter as in Example 7 was coated with 0.52 g of the above γ -Al₂O₃ powder carrying Ag and Sn, dried and heated in the same manner as in Example 7 to obtain a first cleaner portion. The first cleaner portion carrying the Ag-based catalyst was combined with the second cleaner portion of Example 7 carrying the Cu-based catalyst such that the Ag-based catalyst was disposed on the exhaust gas inlet side, and the Cu-based catalyst was disposed on the exhaust gas outlet side. With a test gas having a composition shown in Table 3, the removal ratio of NOx was measured in the same manner as in Example 7. The results are shown in Fig. 4.

Example 9

20 Porous γ -Al₂O₃ powder was impregnated with 2 weight % of Ag by using an aqueous solution of AgNO₃, and 1 weight % of Ga by using an aqueous solution of gallium nitrate, and the same honeycomb-type cordierite filter as in Example 7 was coated with 0.52 g of the above γ -Al₂O₃ powder carrying Ag and Ga, dried and heated in the same manner as in Example 7 to obtain a first cleaner portion. The first cleaner portion carrying the Ag-based catalyst was combined with the second cleaner portion of Example 7 carrying the Cu-based catalyst such that the Ag-based catalyst was disposed on the exhaust gas inlet side, and the Cu-based catalyst was disposed on the exhaust gas outlet side. With a test gas having a composition shown in Table 3, the removal ratio of NOx was measured in the same manner as in Example 7. The results are shown in Fig. 4.

Comparative Example 7

30 1.04 g of porous γ -alumina powder carrying 2 weight % of Ag and 1 weight % of In prepared in the same manner as in Example 7 was coated onto a honeycomb-type cordierite filter which was as long as double that of the honeycomb-type cordierite filter used in Example 7 to obtain an exhaust gas cleaner. This exhaust gas cleaner was set in a reactor pipe in the same manner as in Example 7 to measure the removal ratio of NOx from a test gas having a composition shown in Table 3. The results are shown in Fig. 4.

Comparative Example 8

35 1.04 g of porous γ -alumina powder carrying 10 weight % of Cu, 0.4 weight % of La and 0.4 weight % of Cs prepared in the same manner as in Example 7 was coated onto a honeycomb-type cordierite filter which was as long as double that of the honeycomb-type cordierite filter used in Example 7 to obtain an exhaust gas cleaner. This exhaust gas cleaner was set in a reactor pipe in the same manner as in Example 7 to measure the removal ratio of NOx from a test gas having a composition shown in Table 3. The results are shown in Fig. 4.

45 As is clear from the above, the NOx was well removed in a wide temperature range in Examples 7-9 in which the Ag-based catalyst and the Cu-based catalyst were combined. On the other hand, a temperature range in which the removal ratio of NOx was high was narrow in Comparative Examples 7 and 8 in which either one of the Ag-based catalyst and the Cu-based catalyst was omitted.

Example 10

50 10 g of commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in a mixed aqueous solution of silver nitrate and copper nitrate, dried at 70°C and heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in a nitrogen stream containing 5 volume % of hydrogen and finally at 500°C for 2 hours in a nitrogen stream containing 10 volume % of oxygen, to obtain an exhaust gas cleaner in which 2 weight % (on a metal basis) of Ag and 0.1 weight % (on a metal basis) of Cu were supported by the γ -alumina pellets.

55 The exhaust gas cleaner was charged into a reactor pipe, and a test gas having a composition shown in Table 1 below was caused to pass through the reactor pipe at a rate of 1.75 liters per minute (in a standard state), which corresponded to a space velocity of 30,000 h⁻¹ and a contact time of 0.05 sec-g/ml. The temperature of the test gas was kept at 300-600°C in the reactor pipe to cause a reaction between the nitrogen mon-

oxide in the test gas with propylene.

The concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. The results are shown in Fig. 5.

Example 11

Pellets made of porous γ -alumina carrying 4 weight % of Ag and 0.1 weight % of Cu were set in a reactor pipe in the same manner as in Example 10 to measure the removal ratio of NO_x from a test gas having a composition shown in Table 1. The results are shown in Fig. 5.

Example 12

10 g of porous γ -Al₂O₃ powder (average diameter: 40 μ m, specific surface area: 200 m²/g) was immersed in a mixed aqueous solution of silver nitrate and copper nitrate, dried at 70°C and heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in a nitrogen stream containing 5 volume % of hydrogen, to obtain an exhaust gas cleaner in which 2 weight % (on a metal basis) of Ag and 0.1 weight % (on a metal basis) of Cu were supported by the γ -alumina powder.

1 g of the above the γ -alumina powder carrying Ag and Cu was coated onto a commercially available honeycomb-type cordierite filter (diameter: 30 mm, thickness: 12.5 mm, cell number: 400/square inch) by a wash-coat method and heated at 500°C for 2 hours in a nitrogen stream containing 10 volume % of oxygen, to obtain an exhaust gas cleaner carrying the mixed Ag/Cu catalyst for removing the NO_x. With this exhaust gas cleaner, the removal ratio of NO_x was measured in the same manner as in Example 10 except for changing the flow rate of the test gas to 4.4 liters per minute (in a standard state), which corresponded to a space velocity of 30,000 h⁻¹, a contact time of 0.05 sec-g/ml. The results are shown in Fig. 5.

Comparative Example 9

With the γ -alumina pellets (containing no silver and copper) used in Example 10 only, the removal ratio of NO_x from a test gas having a composition shown in Table 1 was measured in the same manner as in Example 11. The results are shown in Fig. 5.

As is clear from the above, the NO_x was well removed at a temperature of 350-600°C in Examples 10-12. On the other hand, the removal ratio of NO_x was low at an exhaust gas temperature of 500°C or lower in the case of the exhaust gas cleaner containing no catalytically active component (Comparative Example 9). Incidentally, the removal ratio of NO_x increased gradually as the exhaust gas temperature exceeded 500°C in Comparative Example 9, but it should be noted that the by-production of carbon monoxide (CO) increased. Such a phenomenon did not take place in Examples 10-12 (producing substantially no carbon monoxide), and carbon dioxide was produced instead.

Example 13

10 g of commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in a mixed aqueous solution of silver nitrate and potassium nitrate, dried at 70°C and heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in a nitrogen stream containing 5 volume % of hydrogen, to obtain an exhaust gas cleaner in which 2 weight % (on a metal basis) of Ag and 0.5 weight % (on a metal basis) of K were supported by the γ -alumina pellets.

The exhaust gas cleaner was charged into a reactor pipe, and a test gas having a composition shown in Table 3 below was caused to pass through the reactor pipe at a rate of 4.4 liters per minute (in a standard state), which corresponded to a space velocity of 30,000 h⁻¹ and a contact time of 0.05 sec-g/ml. The temperature of the test gas was kept at 300-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene.

The concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. The results are shown in Fig. 6.

Example 14

1.3 g of porous γ -alumina powder (average diameter: 40 μ m, specific surface area: 200 m²/g) carrying 2

weight % of Ag and 0.5 weight % of K prepared in the same manner as in Example 13 was coated onto a commercially available honeycomb-type cordierite filter (diameter: 30 mm, thickness: 12.5 mm) by a wash-coat method. With the resulting exhaust gas cleaner, the removal ratio of NO_x was measured under the same conditions as in Example 13 (space velocity of 30,000 h⁻¹). The results are shown in Fig. 6.

Comparative Example 10

Porous γ -alumina pellets carrying only 2 weight % of Ag were prepared and used to measure the removal ratio of NO_x in the same manner as in Example 13. The results are shown in Fig. 6.

Comparative Example 11

Porous γ -alumina pellets carrying 2 weight % of Ag and 0.5 weight % of Ce were prepared and used to measure the removal ratio of NO_x in the same manner as in Example 13. The results are shown in Fig. 6.

As is clear from the above, the NO_x was well removed at a temperature of 400-600°C in Examples 13 and 14. On the other hand, the removal ratio of NO_x was low at an exhaust gas temperature of 500°C or lower in the case of the exhaust gas cleaner containing only Ag component (Comparative Example 10). Also, in the case of the exhaust gas cleaner containing Ag component and a rare earth metal (Comparative Example 11), high removal ratio of NO_x could not be achieved in the overall temperature range.

Example 15

10 g of commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in an aqueous solution of AgNO₃, dried at 70°C and heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in a nitrogen stream containing 5 volume % of hydrogen. They were then immersed in an aqueous solution of chloroplatinic acid and dried at 70°C and heated at 600°C for 2 hours to produce an exhaust gas cleaner in which 5 weight % (on a metal basis) of Ag and 0.01 weight % (on a metal basis) of Pt were supported by the γ -alumina pellets.

3.6 g of the resulting exhaust gas cleaner was charged into a reactor pipe, and a test gas having a composition shown in Table 3 below was caused to pass through the reactor pipe at a rate of 4.4 liters per minute (in a standard state), which corresponded to a space velocity of 30,000 h⁻¹ and a contact time of 0.05 sec-g/ml. The temperature of the test gas was kept at 300-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene.

The concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. The results are shown in Fig. 7.

Example 16

1.3 g of porous γ -alumina powder (average diameter: 40 μ m, specific surface area: 200 m²/g) carrying 5 weight % of Ag and 0.01 weight % of Pt was prepared in the same manner as in Example 15, and coated onto a commercially available honeycomb-type cordierite filter (diameter: 30 mm, thickness: 12.5 mm) by a wash-coat method. With the resulting exhaust gas cleaner, the removal ratio of NO_x was measured under the same conditions as in Example 15 (space velocity of 30,000 h⁻¹). The results are shown in Fig. 7.

Comparative Example 12

Porous γ -alumina pellets carrying only 5 weight % of Ag were prepared and used to measure the removal ratio of NO_x in the same manner as in Example 15. The results are shown in Fig. 7.

Comparative Example 13

Porous γ -alumina pellets carrying 5 weight % of Ag and 0.15 weight % of Pt were prepared and used to measure the removal ratio of NO_x in the same manner as in Example 15. The results are shown in Fig. 7.

Comparative Example 14

Titania pellets were impregnated with 5 weight % of Ag and 0.01 weight % of Pt and used to measure the

removal ratio of NO_x in the same manner as in Example 15. The results are shown in Fig. 7.

As is clear from the above, the NO_x was well removed at a temperature of 300-600°C in Examples 15 and 16. On the other hand, the removal ratio of NO_x was low at an exhaust gas temperature of 500°C or lower in the case of the exhaust gas cleaner containing only Ag component (Comparative Example 12). Also, in the case of the exhaust gas cleaner containing Ag and an excess amount of Pt (Comparative Example 13), a high removal ratio of NO_x could not be achieved in the overall temperature range. Further, when titania was used instead of alumina as a porous inorganic oxide, the removal ratio of NO_x was low (Comparative Example 14).

Example 17

10 g of commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in an aqueous solution of ammonium molybdate, dried at 70°C and heated at 600°C. They were then immersed in an aqueous solution of silver nitrate, dried at 70°C, heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in a nitrogen stream containing 5 volume % of hydrogen and heated at 500°C for 2 hours in a nitrogen stream containing 10 volume % of oxygen to produce an exhaust gas cleaner in which 5 weight % (on a metal basis) of Ag and 0.5 weight % (on a metal basis) of Mo were supported by the γ -alumina pellets.

3.6 g of the resulting exhaust gas cleaner was charged into a reactor pipe, and a test gas having a composition shown in Table 3 below was caused to pass through the reactor pipe at a rate of 4.4 liters per minute (in a standard state), which corresponded to a space velocity of 30,000 h⁻¹ and a contact time of 0.05 sec-g/ml. The temperature of the test gas was kept at 300-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene.

The concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. The results are shown in Fig. 8.

Example 18

1.3 g of porous γ -alumina powder (average diameter: 40 μ m, specific surface area: 200 m²/g) carrying 5 weight % of Ag and 0.5 weight % of Mo was prepared in the same manner as in Example 17, and coated onto a commercially available honeycomb-type cordierite filter (diameter: 30 mm, thickness: 12.5 mm) by a wash-coat method. With the resulting exhaust gas cleaner, the removal ratio of NO_x was measured under the same conditions as in Example 17 (space velocity of 30,000 h⁻¹). The results are shown in Fig. 8.

Comparative Example 15

Porous γ -alumina pellets carrying only 5 weight % of Ag were prepared and used to measure the removal ratio of NO_x in the same manner as in Example 17. The results are shown in Fig. 8.

Comparative Example 16

Porous γ -alumina pellets carrying 5 weight % of Ag and 5 weight % of Mo were prepared and used to measure the removal ratio of NO_x in the same manner as in Example 17. The results are shown in Fig. 8.

As is clear from the above, the NO_x was well removed at a temperature of 300-600°C in Examples 17 and 18. On the other hand, the removal ratio of NO_x was low at an exhaust gas temperature of 450°C or lower in the case of the exhaust gas cleaner containing only Ag component (Comparative Example 15). Also, in the case of the exhaust gas cleaner containing Ag and an excess amount of Mo (Comparative Example 16), a high removal ratio of NO_x could not be achieved in the overall temperature range.

Example 19

10 g of commercially available pellets made of porous γ -alumina (diameter: 1.5 mm, length: about 6 mm, specific surface area: 200 m²/g) were immersed in an aqueous solution of gallium nitrate and an aqueous solution of silver nitrate, dried at 70°C and heated at 150°C, 200°C, 300°C, 400°C, 500°C and 600°C each for 2 hours in the air, to produce an exhaust gas cleaner in which 2.5 weight % (on a metal basis) of Ag and 2.5 weight % (on a metal basis) of Ga were supported by the γ -alumina pellets.

3.6 g of the resulting exhaust gas cleaner was charged into a reactor pipe, and a test gas having a composition shown in Table 3 below was caused to pass through the reactor pipe at a rate of 4.4 liters per minute

(in a standard state), which corresponded to a space velocity of 30,000 h⁻¹ and a contact time of 0.05 sec-g/ml. The temperature of the test gas was kept at 300-600°C in the reactor pipe to cause a reaction between the nitrogen monoxide in the test gas with propylene.

The concentration of NO_x (sum of nitrogen monoxide and nitrogen dioxide) in the test gas after passing through the exhaust gas cleaner was measured by a chemiluminescence analyzer to determine the removal ratio of NO_x. The results are shown in Fig. 9.

Example 20

Porous γ -alumina pellets carrying 2.5 weight % of Ag and 2.5 weight % of Sn was prepared in the same manner as in Example 19, and used to measure the removal ratio of NO_x from the test gas having a composition shown in Table 3. The results are shown in Fig. 9.

Example 21

About 1 g of porous γ -alumina powder (specific surface area: 200 m²/g) carrying 2.5 weight % (on a metal basis) of Ag and 2.5 weight % (on a metal basis) of Ga was prepared in the same manner as in Example 19, and coated onto a commercially available honeycomb-type cordierite filter (diameter: 30 mm, thickness: 12.5 mm) by a wash-coat method. With the resulting exhaust gas cleaner, the removal ratio of NO_x was measured under the same conditions as in Example 19 (space velocity of 30,000 h⁻¹). The results are shown in Fig. 9.

Comparative Example 17

Only the same porous γ -alumina pellets as in Example 19 were used to measure the removal ratio of NO_x. The results are shown in Fig. 9.

As is clear from the above, the NO_x was well removed in a wide temperature range in Examples 19-21 using the exhaust gas cleaner containing Ag and Sn, etc. On the other hand, the removal ratio of NO_x was extremely low at an exhaust gas temperature of 400°C or lower in Comparative Examples 17.

As described above in detail, by the exhaust gas cleaner according to the present invention, NO_x can efficiently be removed from the exhaust gas having an excess oxygen concentration in a wide temperature range even when about 10% of water is contained in the exhaust gas. Further, in the case of the mixed catalyst-type exhaust gas cleaner, the NO_x-removing temperature can be as low as about 500°C or lower.

The exhaust gas cleaner of the present invention is effective for cleaning exhaust gases such as those discharged from various combustors, automobile engines, etc.

Claims

1. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises a mixture of (1) a first catalyst comprising 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body; and (2) a second catalyst comprising 0.5-20 weight % (on a metal basis) of second catalytically active components supported by a porous inorganic oxide body, said second catalytically active components consisting essentially of (i) at least one alkali metal element; (ii) at least one element selected from the group consisting of Cu, Co, Mn and V; and (iii) at least one rare earth element, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body.
2. The exhaust gas cleaner according to claim 1, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
3. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising a mixture of (1) a first catalyst comprising 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body; and (2) a second catalyst comprising 0.5-20 weight % (on a metal basis) of second catalytically active components supported by a porous inorganic oxide body, said second catalytically active components consisting essentially of (i) at

- least one alkali metal element; (ii) at least one element selected from the group consisting of Cu, Co, Mn and V; and (iii) at least one rare earth element, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into said exhaust gas on the upstream side of said exhaust gas cleaner; and (c) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby removing said nitrogen oxides.
4. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises a cleaner substrate made of ceramics or metals, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) said second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body.
 5. The exhaust gas cleaner according to claim 4, wherein said second catalytically active components further contain 4 weight % or less (on a metal basis), based on said porous inorganic oxide body, of at least one element selected from the group consisting of alkali metal elements and rare earth elements.
 6. The exhaust gas cleaner according to claim 4, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
 7. The exhaust gas cleaner according to claim 5, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
 8. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising a cleaner substrate made of ceramics or metals, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) said second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into said exhaust gas on the upstream side of said exhaust gas cleaner; and (c) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby removing said nitrogen oxides.
 9. The method of cleaning an exhaust gas according to claim 8, wherein said second catalytically active components further contain 4 weight % or less (on a metal basis), based on said porous inorganic oxide body, of at least one element selected from the group consisting of alkali metal elements and rare earth elements.
 10. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises a cleaner substrate, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) said second catalyst comprises 2 weight % (on a metal basis) or less of a second catalytically active component supported by a porous inorganic oxide body, said second catalytically active component consisting essentially of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body.
 11. The exhaust gas cleaner according to claim 10, wherein said porous inorganic oxide body for said first and second catalysts is porous inorganic oxide powder coated onto said cleaner substrate made of cer-

amics or metals.

12. The exhaust gas cleaner according to claim 10, wherein said porous inorganic oxide body for said first and second catalysts is in the form of pellet or granule.
- 5 13. The exhaust gas cleaner according to claim 10, wherein said porous inorganic oxide body for said first catalyst is made of alumina or an alumina composite oxide, and said porous inorganic oxide body for said second catalyst is made of alumina, titania, zirconia or an a composite oxide thereof.
- 10 14. A method of cleaning an exhaust gas containing nitrogen oxides, carbon monoxide, hydrocarbons and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising a cleaner substrate, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.1-15 weight % (on a metal basis) of a first catalytically active component consisting essentially of Ag supported by a porous inorganic oxide body, and (2) said second catalyst comprises 2 weight % (on a metal basis) or less of a second catalytically active component supported by a porous inorganic oxide body, said second catalytically active component consisting essentially of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into said exhaust gas on the upstream side of said exhaust gas cleaner; and (c) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby removing said nitrogen oxides, carbon monoxide and hydrocarbons.
- 20 15. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises a cleaner substrate, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.2-20 weight % (on a metal basis) of first catalytically active components supported by a porous inorganic oxide body, said first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) said second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body.
- 25 16. The exhaust gas cleaner according to claim 15, wherein said second catalytically active components further contain 4 weight % or less (on a metal basis), based on said porous inorganic oxide body, of at least one element selected from the group consisting of alkali metal elements and rare earth elements.
- 30 17. The exhaust gas cleaner according to claim 15, wherein said porous inorganic oxide body for said first and second catalysts is porous inorganic oxide powder coated onto said cleaner substrate made of ceramics or metals.
- 35 18. The exhaust gas cleaner according to claim 16, wherein said porous inorganic oxide body for said first and second catalysts is porous inorganic oxide powder coated onto said cleaner substrate made of ceramics or metals.
- 40 19. The exhaust gas cleaner according to claim 15, wherein said porous inorganic oxide body for said first and second catalysts is in the form of pellet or granule.
- 45 20. The exhaust gas cleaner according to claim 16 wherein said porous inorganic oxide body for said first and second catalysts is in the form of pellet or granule.
- 50 21. The exhaust gas cleaner according to claim 15, wherein said porous inorganic oxide body is made of alumina, titania, zirconia or an a composite oxide thereof.
- 55 22. The exhaust gas cleaner according to claim 16, wherein said porous inorganic oxide body is made of alumina, titania, zirconia or an a composite oxide thereof.

23. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising a cleaner substrate, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.2-20 weight % (on a metal basis) of first catalytically active components supported by a porous inorganic oxide body, said first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) said second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body; (b) introducing hydrocarbons and/or oxygen-containing organic compounds into said exhaust gas on the upstream side of said exhaust gas cleaner; and (c) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby removing said nitrogen oxides.
24. The method according to claim 23, wherein said second catalytically active components further contain 4 weight % or less (on a metal basis), based on said porous inorganic oxide body, of at least one element selected from the group consisting of alkali metal elements and rare earth elements.
25. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising a cleaner substrate, a first catalyst supported by said cleaner substrate on the exhaust gas inlet side thereof, and a second catalyst supported by said cleaner substrate on the exhaust gas outlet side thereof, wherein (1) said first catalyst comprises 0.2-20 weight % (on a metal basis) of first catalytically active components supported by a porous inorganic oxide body, said first catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (2) said second catalyst comprises 0.1-15 weight % (on a metal basis) of a second catalytically active component consisting essentially of Cu supported by a porous inorganic oxide body, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body; and (b) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between said nitrogen oxides and hydrocarbons remaining in said exhaust gas to remove said nitrogen oxides.
26. The method according to claim 25, wherein said second catalytically active components further contain 4 weight % or less (on a metal basis), based on said porous inorganic oxide body, of at least one element selected from the group consisting of alkali metal elements and rare earth elements.
27. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis) of Ag, and (ii) 2 weight % or less (on a metal basis) of Cu, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body.
28. The exhaust gas cleaner according to claim 27, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
29. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis) of Ag, and (ii) 2 weight % or less (on a metal basis) of Cu, all of said percentages being based on the total amount (100 weight %) of said porous inorganic oxide body; (b) introducing 400 volume % or less, based on said nitrogen oxides in said exhaust gas, of hydrocarbons which are gaseous in a standard state into said exhaust gas on the upstream side of said exhaust gas cleaner; and (c) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 250-600°C, thereby removing said nitrogen oxides.

30. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on said porous inorganic oxide body, of Ag, and (ii) 50 weight % or less (on a metal basis), based on said Ag, of at least one element selected from the group consisting of alkali metal elements and alkali earth metal elements.
31. The exhaust gas cleaner according to claim 30, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
32. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on said porous inorganic oxide body, of Ag, and (ii) 50 weight % or less (on a metal basis), based on said Ag, of at least one element selected from the group consisting of alkali metal elements and alkali earth metal elements; and (b) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between said nitrogen oxides and hydrocarbons remaining in said exhaust gas to remove said nitrogen oxides.
33. The method according to claim 32, wherein hydrocarbons and/or oxygen-containing organic compounds in amounts of 5 times or less those of said nitrogen oxides in said exhaust gas are introduced into said exhaust gas on the upstream side of said exhaust gas cleaner.
34. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on said porous inorganic oxide body, of Ag, and (ii) 2 weight % or less (on a metal basis), based on said Ag, of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir.
35. The exhaust gas cleaner according to claim 34, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
36. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on said porous inorganic oxide body, of Ag, and (ii) 2 weight % or less (on a metal basis), based on said Ag, of at least one element selected from the group consisting of Pt, Pd, Ru, Rh and Ir; and (b) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between said nitrogen oxides and hydrocarbons remaining in said exhaust gas to remove said nitrogen oxides.
37. The method according to claim 36, wherein hydrocarbons and/or oxygen-containing organic compounds in amounts of 5 times or less those of said nitrogen oxides in said exhaust gas are introduced into said exhaust gas on the upstream side of said exhaust gas cleaner.
38. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on said porous inorganic oxide body, of Ag, and (ii) 20 weight % or less (on a metal basis), based on said Ag, of at least one element selected from the group consisting of Mo, W, Cr, Ni, Mn and Co.
39. The exhaust gas cleaner according to claim 38, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.

- 5 40. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of (i) 0.1-15 weight % (on a metal basis), based on said porous inorganic oxide body, of Ag, and (ii) 20 weight % or less (on a metal basis), based on said Ag, of at least one element selected from the group consisting of Mo, W, Cr, Ni, Mn and Co; and (b) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between said nitrogen oxides and hydrocarbons remaining in said exhaust gas to remove said nitrogen oxides.
- 10 41. The method according to claim 40, wherein hydrocarbons and/or oxygen-containing organic compounds in amounts of 5 times or less those of said nitrogen oxides in said exhaust gas are introduced into said exhaust gas on the upstream side of said exhaust gas cleaner.
- 15 42. An exhaust gas cleaner for cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In.
- 20 43. The exhaust gas cleaner according to claim 42, wherein said porous inorganic oxide body is made of alumina or a composite oxide thereof.
- 25 44. The exhaust gas cleaner according to claim 42, wherein the total amount of said catalytically active components is 0.2-20 weight % (on a metal basis), based on said porous inorganic oxide body.
- 30 45. A method of cleaning an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in said exhaust gas, which comprises (a) disposing an exhaust gas cleaner in a flow path of said exhaust gas, said exhaust gas cleaner comprising catalytically active components supported by a porous inorganic oxide body, said catalytically active components consisting essentially of Ag and at least one element selected from the group consisting of Sn, Al, Ga and In; and (b) bringing said exhaust gas into contact with said exhaust gas cleaner at a temperature of 200-600°C, thereby causing a reaction between said nitrogen oxides and hydrocarbons remaining in said exhaust gas to remove said nitrogen oxides.
- 35 46. The method according to claim 45, wherein hydrocarbons and/or oxygen-containing organic compounds in amounts of 0.1-5 times those of said nitrogen oxides in said exhaust gas are introduced into said exhaust gas on the upstream side of said exhaust gas cleaner.

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FIG. 1

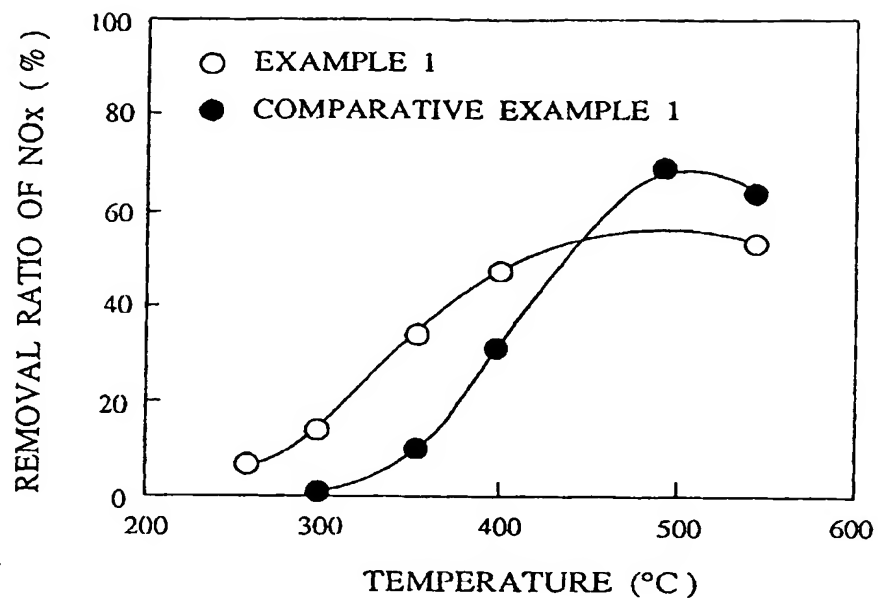


FIG. 2

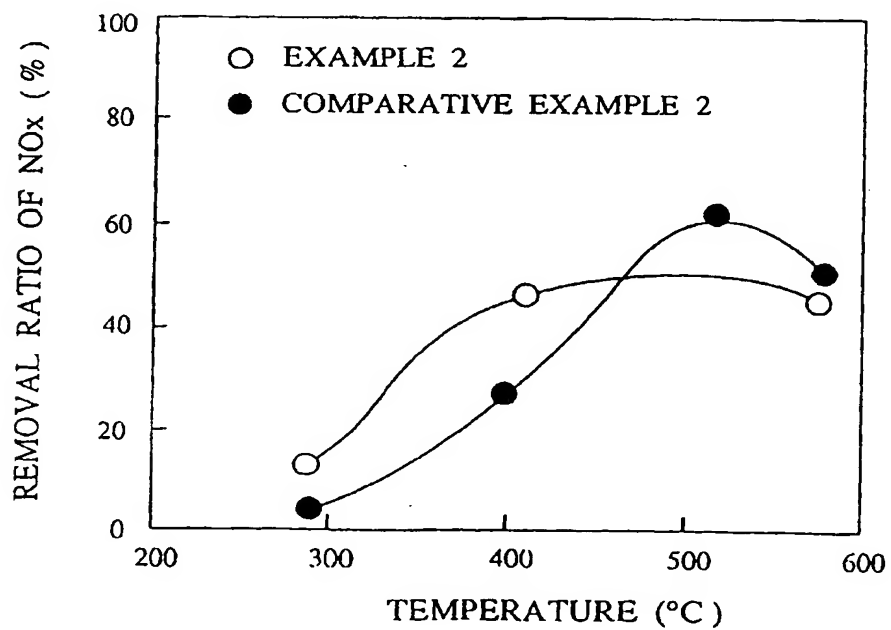


FIG. 3

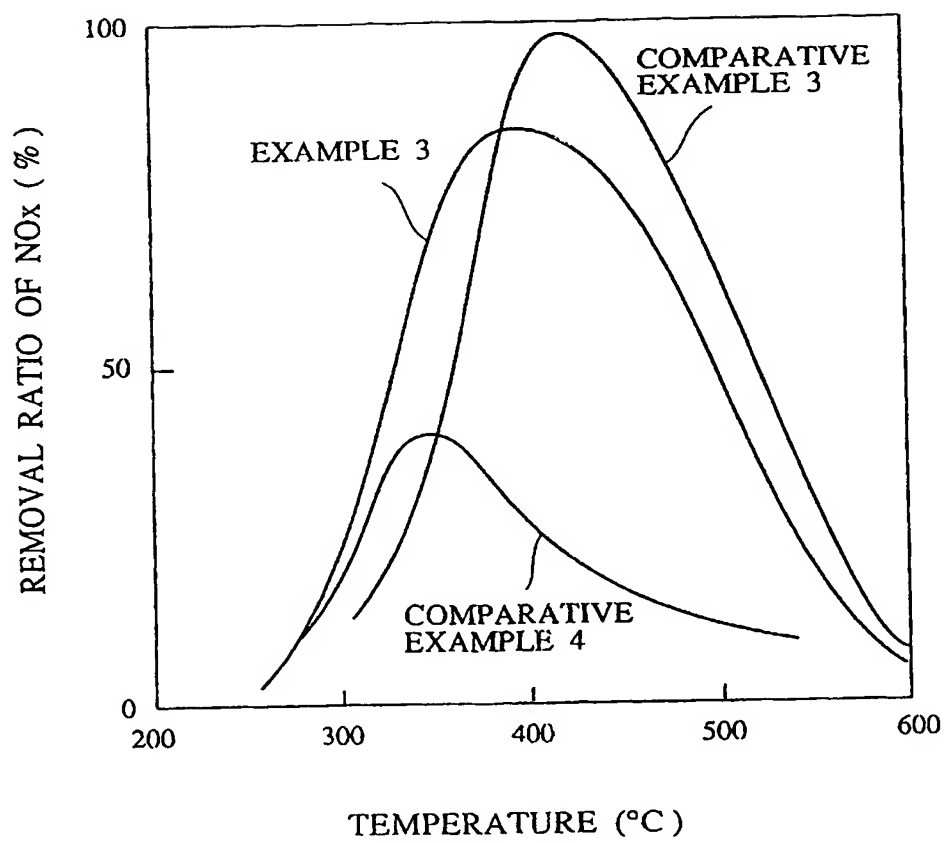


FIG. 4

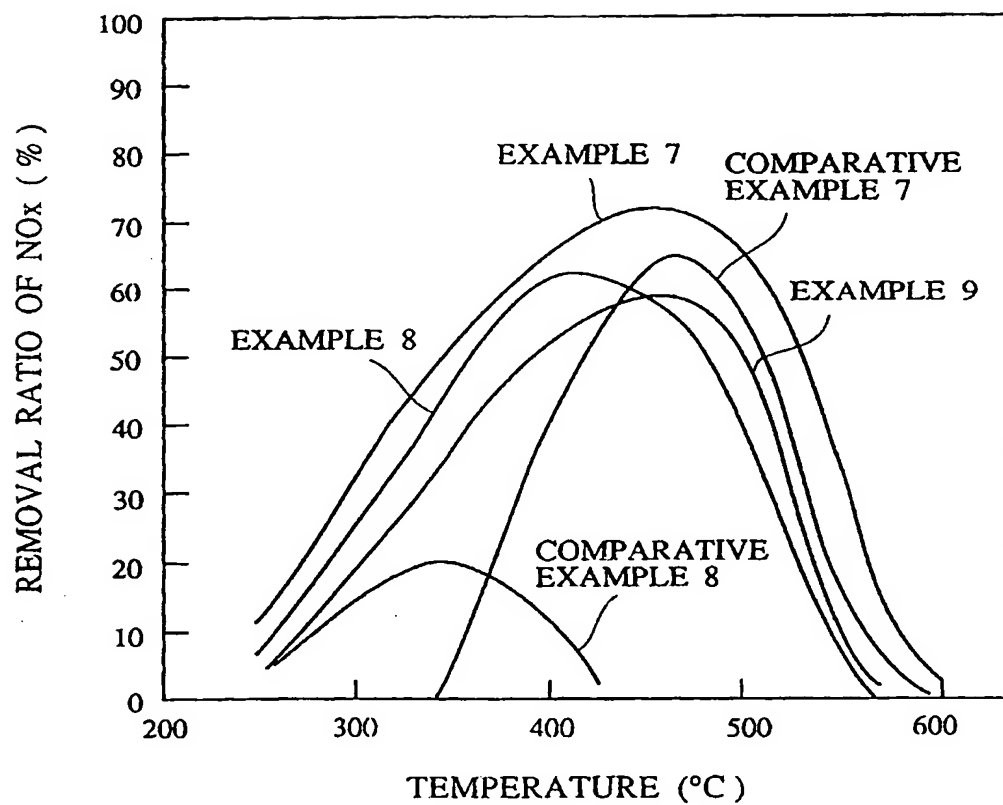


FIG. 5

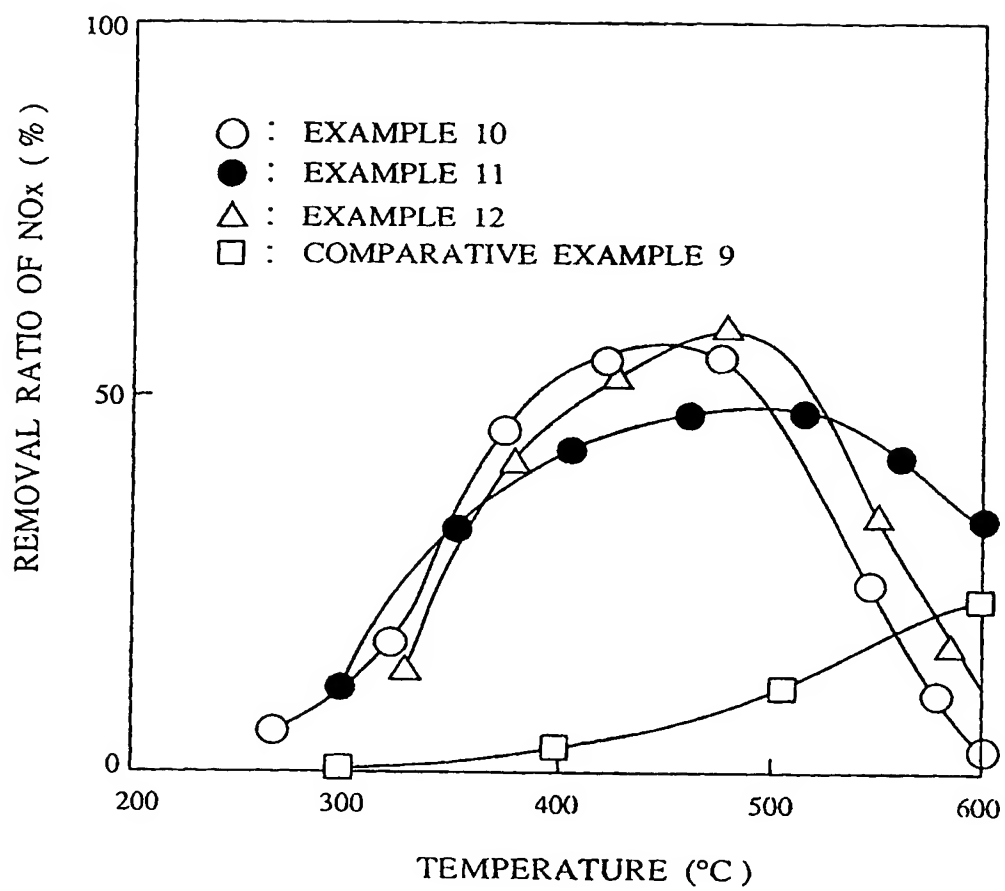


FIG. 6

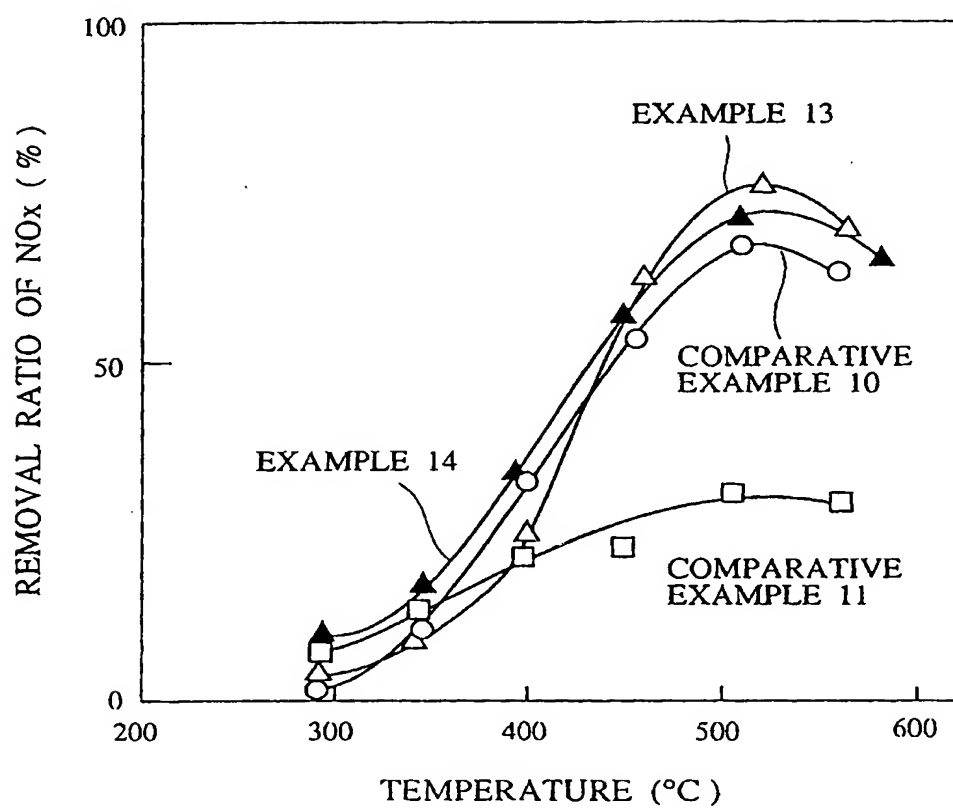


FIG. 7

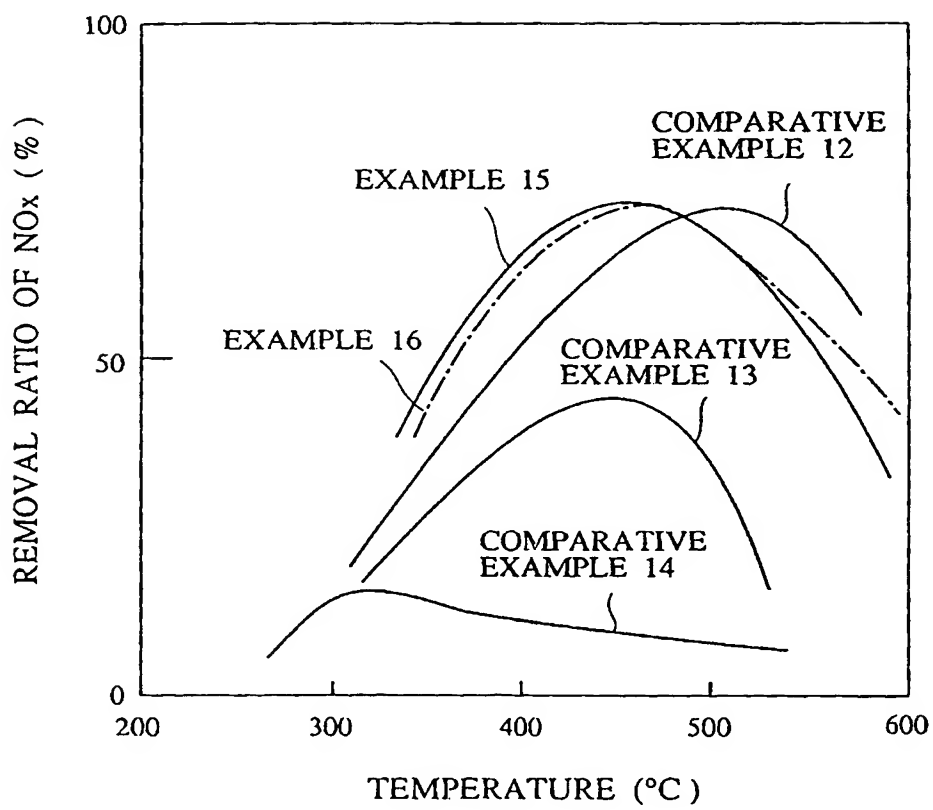


FIG. 8

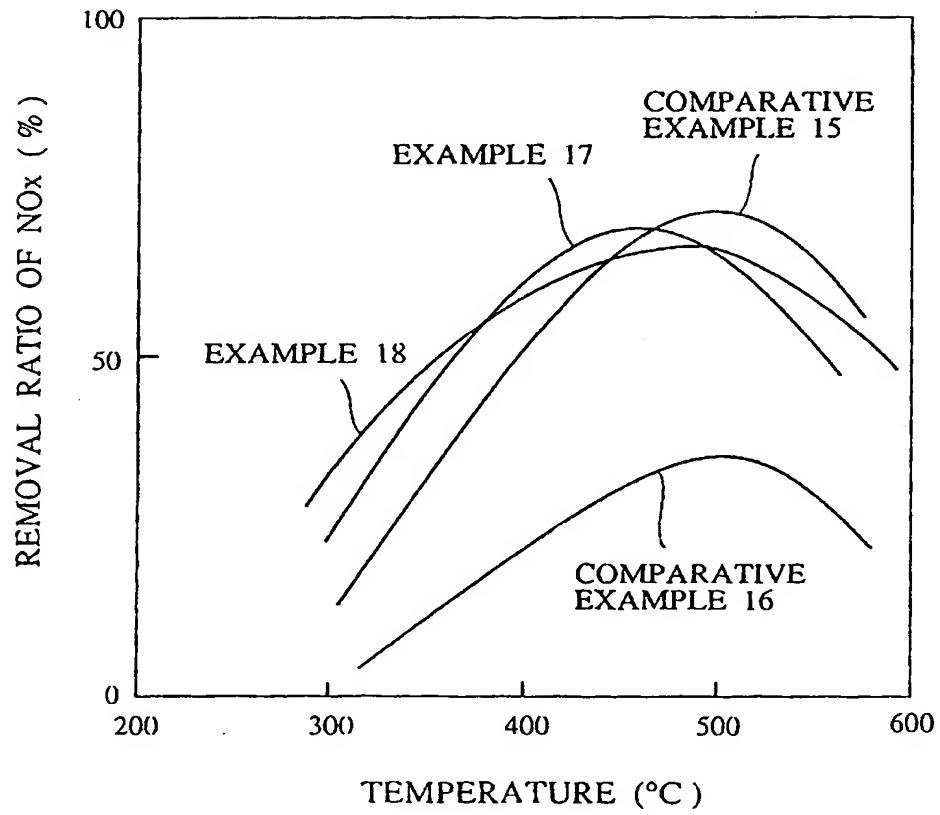
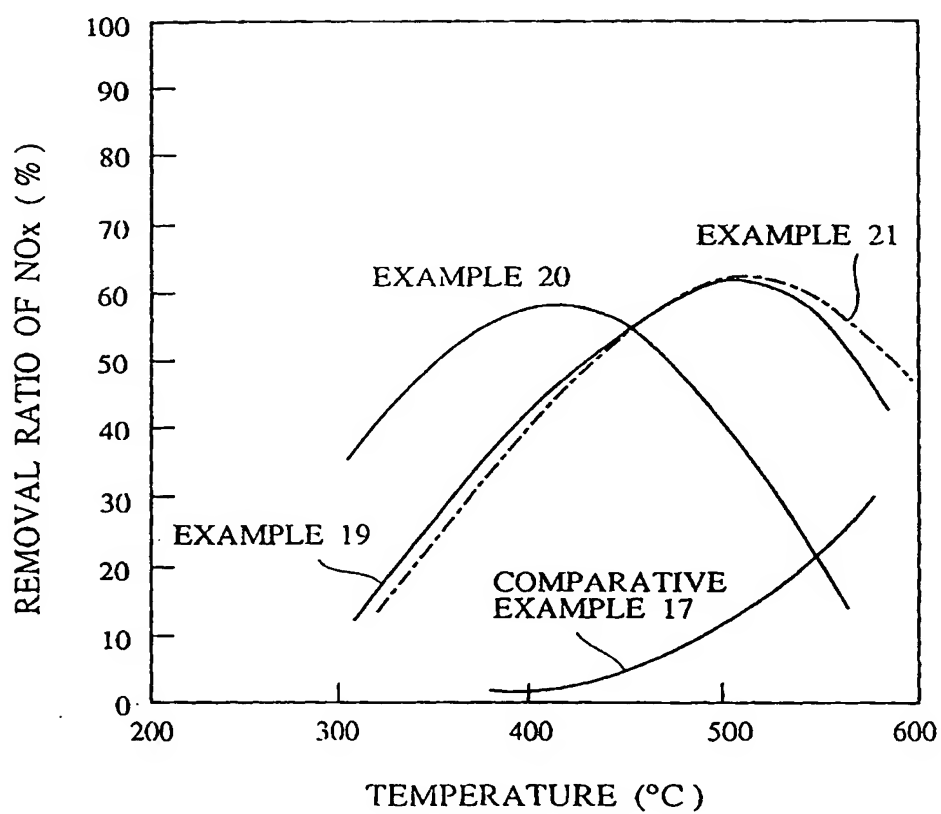


FIG. 9





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European Patent Office
Office européen des brevets



Publication number : **0 577 438 A3**

(12)

EUROPEAN PATENT APPLICATION

(21) Application number : **93305235.9**

(22) Date of filing : **02.07.93**

(51) Int. Cl.⁵ : **B01D 53/36, B01J 23/89,
B01J 23/50**

- (30) Priority : **03.07.92 JP 200638/92**
05.10.92 JP 290760/92
15.10.92 JP 302840/92
15.10.92 JP 302891/92
15.10.92 JP 302899/92
23.10.92 JP 309433/92
13.11.92 JP 328895/92
20.11.92 JP 335478/92
24.11.92 JP 336583/92
25.12.92 JP 358235/92
25.12.92 JP 358316/92
25.12.92 JP 358348/92
13.01.93 JP 20566/93
- (43) Date of publication of application :
05.01.94 Bulletin 94/01
- (84) Designated Contracting States :
DE FR GB
- (88) Date of deferred publication of search report :
25.05.94 Bulletin 94/21
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(54) Exhaust gas cleaner and method of cleaning exhaust gas.

- (57) Nitrogen oxides are removed from an exhaust gas containing nitrogen oxides and oxygen in an amount larger than its stoichiometric amount relative to unburned components in the exhaust gas, by using an exhaust gas cleaner having Ag supported by a porous inorganic oxide body and second catalyst containing second catalytically active components supported by a porous inorganic oxide body. The second catalytically active components consist essentially of Cu and/or other metals such as alkali metal elements, rare earth elements, etc.

EP 0 577 438 A3



European Patent
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EUROPEAN SEARCH REPORT

Application Number
EP 93 30 5235 9

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 5)
X	GB-A-2 248 194 (KK RIKEN) * claims 1-18 *	1-46	B01D53/36 B01J23/89 B01J23/50
X	EP-A-0 362 960 (SAKAI CHEMICAL IND. CO.) * claims 1-8 *	1-46	
X	DE-A-40 08 371 (KK RIKEN) * the whole document *	1-46	
X	US-A-3 857 921 (ASAKI KASEI KOGYO KK) * claims 1-4 *	1-46	
P, A	EP-A-0 498 325 (IDEMITSU KOSAN CO. LTD.) 12 August 1992 * page 3, line 19 - page 4, line 18; claims 1-12 *	1-46	
			TECHNICAL FIELDS SEARCHED (Int. Cl. 5)
			B01D B01J
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 31 March 1994	Examiner Eijkenboom, A
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons * : member of the same patent family, corresponding document</p>			

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